FIELD BOOK

S. 1133

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

SHAW'S
PIONEERS
SINCE 1831

Field Book

No. S 1135

158

MADE IN 88 LEAVES

A Product of Wilson-Jones Co.
Made in U. S. A.

Book 128
Ck'd

copies in
Steno
book

C.H. #4

Chardon Auburn Center Road
IVPSO Project 1012-A
(Copied)

21+87.00 Δ = 00°10'00" Lt.

NOTE: Plans in basement
See File 1012-A

17+0 Spk (chaining only) May '51

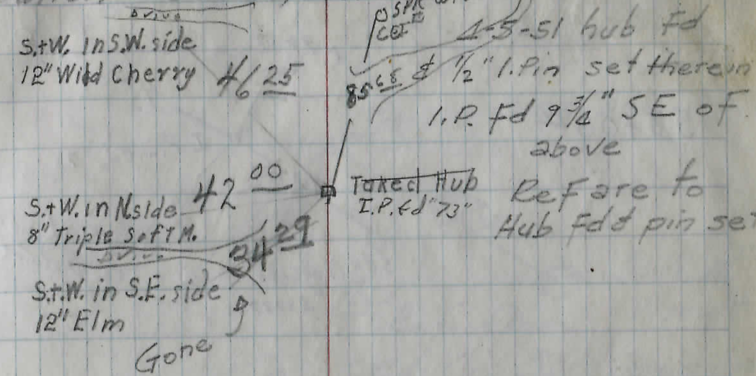
9+77.05 tang.

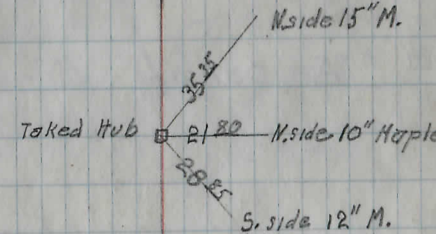
0+00 tang.

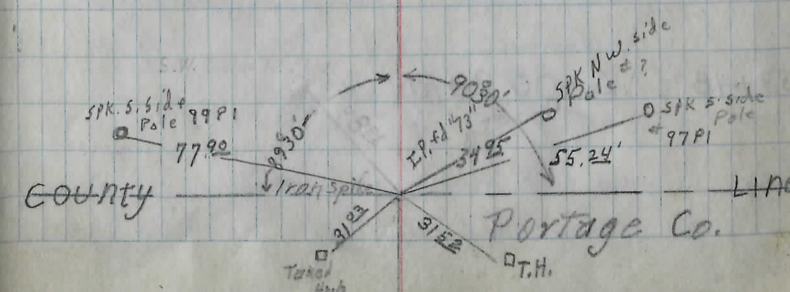
County line to Auburn Ctr.

Gea # 1528

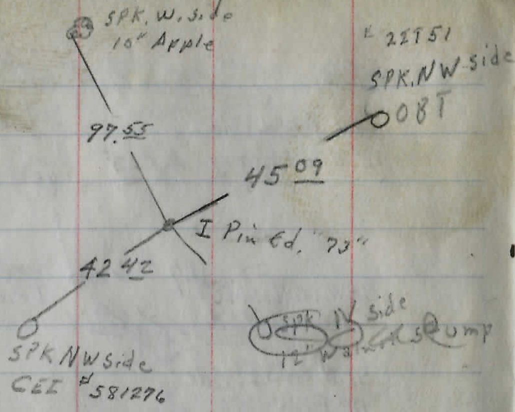
℄ Location Sec. A, B & C.







91.06



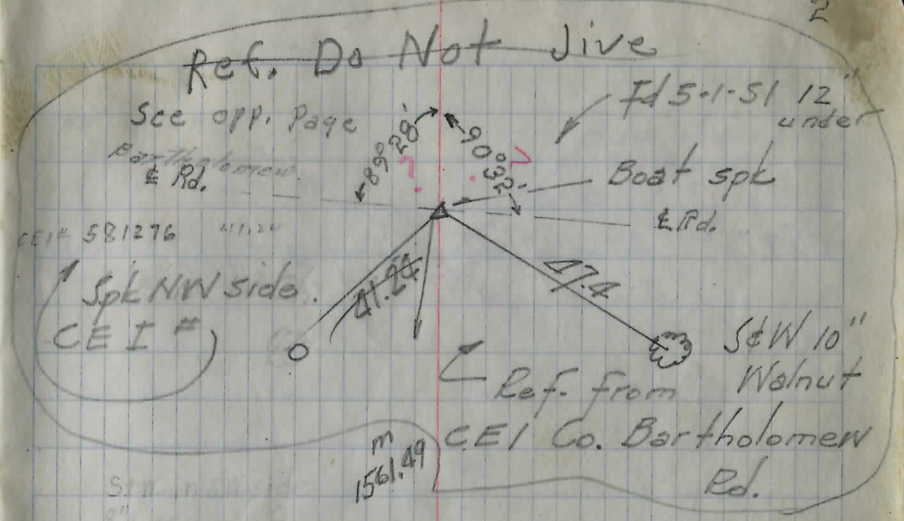
58+08.94

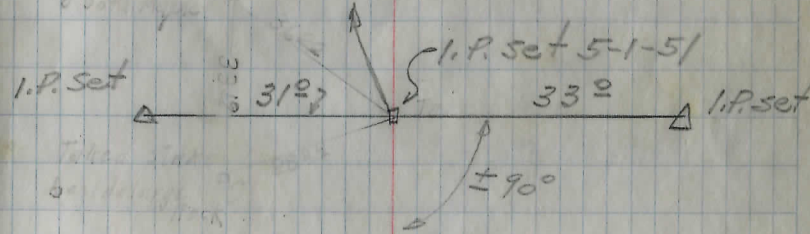
4248.04
1561.49
5809.53

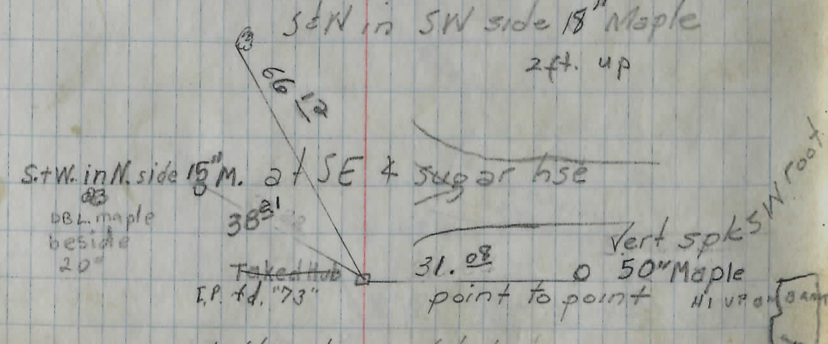
42+48.04 Δ = tang.

51.60

33+48.40 Δ = 00° 20' Rt.





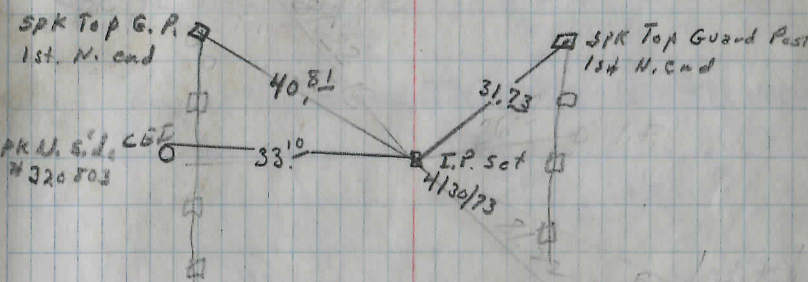


4-7-51 bolt set in old hub fd
I.P. fd 0.78 SW of above

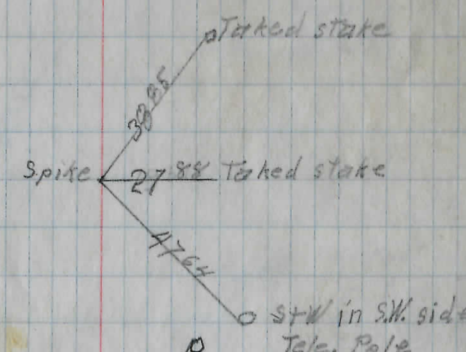
85+76.18 Δ = 00°42' Lt.
5-2-51 I.P. set in old hub

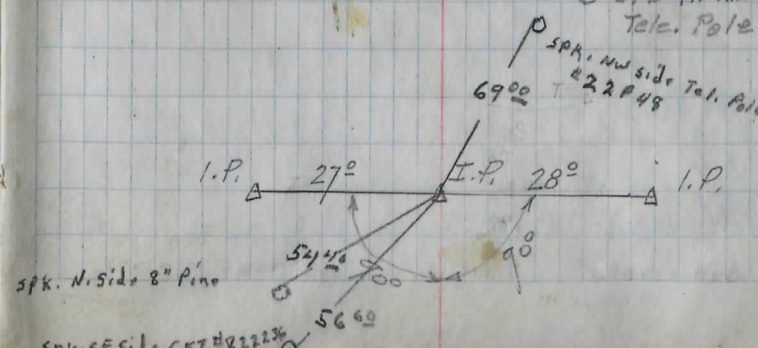
73+01.15 Δ Tang.

62+17.18 Δ = 00°12' Lt.
I.P. set 5-1-51
I.P. set 4/30/73



m 1951
1264.4





109+53.76 Δ=00°38' Rt.

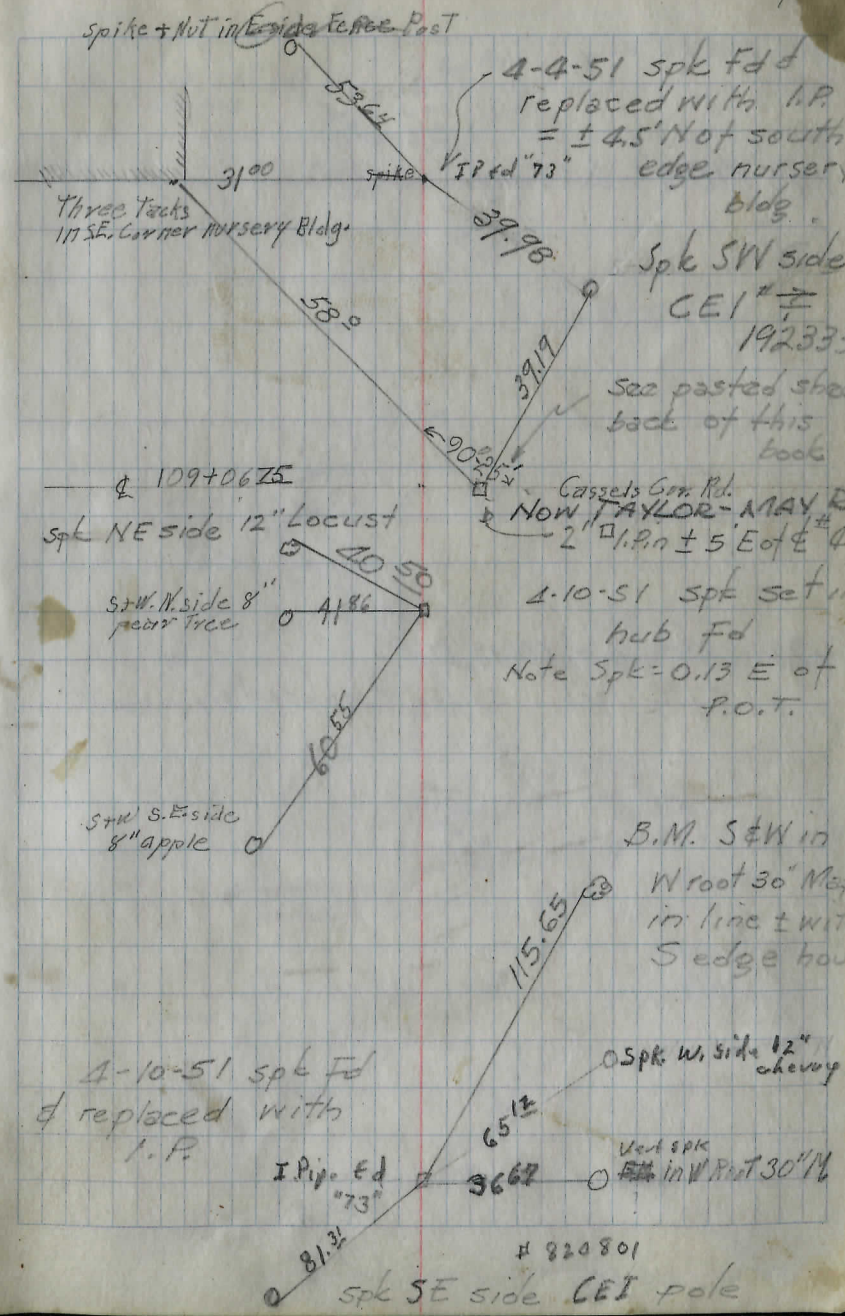
103 43.61
614.88
109 58.49

m 1951
614.88

103+43 ℄ Δ=tang.

28.74

90+71.86 Δ=1°-08" Rt.

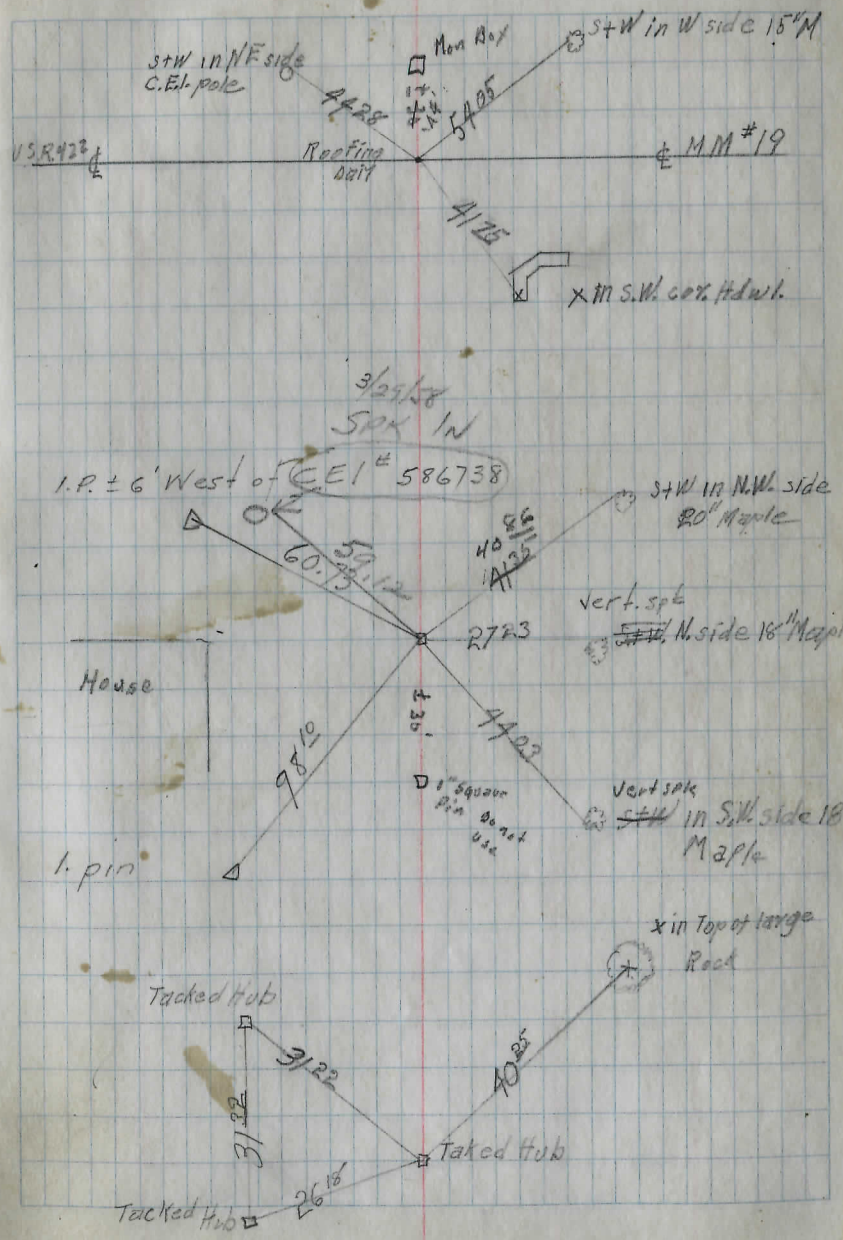


145+10.62 △ = tang.

134+48.82 △ = 00°13' Lt.
+47.20 1951 Spk fd & replaced with bolt

116+75.99 △ = tang.

spk 116+0 ok line & dist



Bench marks

	Description
BM #1	S+W in E. root 15" Elm
* #2	S+W in W. root 4'-00 chestnut
* #3	S+W in W. root 24" Maple
#4	S+W in S.W. root 12" Walnut Fd 1951
#5	S+W in W. root 36" Maple (New #5 = 1128.00
#6	S+W in W. root 30" Maple Fd 1951
#7	S+W in W. root 30" Maple GONE
#8	X on large rock 26' Rt.
#9	S+W in W. root 24" Maple 29' Rt.
#10	S+W in SW. root 24" Maple 26' Rt.
#11	X on S.E. cor. N. Hdwll Culvert

* B.M. #2 Replaced per print WPSD 1012A =
Bent over spike E. Side 10" Cherry Sta 22+08
35' left 1.5' up Elv = 1171.32 (only scar visible)
* B.M. #3 Now - Bent Spk NE. Root 14" Maple 36+95 27' left

Station		elevation
0+68	–	1164.65
21+00	–	1170.38
41+25	–	1163.87
57+90	–	1161.87
80+22	–	1128.04
91+83	–	1159.50
100+30	–	1202.71
117+05	–	1235.64
130+19 = 2.5+ N. of S. line Fox farm	–	1236.91
138+38	–	1232.55
145+70	–	1232.03

= 1161.98 (New Spk (1951) set Elv 1162.12)

1-31-49 PM F E Z rod
F.C.P

B.M.	7.21	107.21	100.00	Assmd.
set				
		9.30	97.91	
		10.45	96.76	
		9.26	97.95	
	±	9.5	97.71	

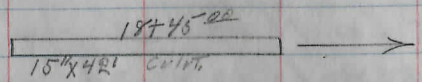
Fred Dietz Auburn Trustee
[illegible] may } viewed some.

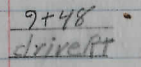
C.R. Hertel pond problem E. side Chardon-Auburn Road = ±½ mile S. of Auburn Center

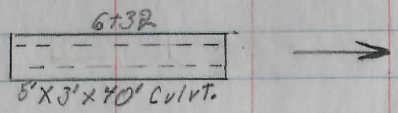
±E. Rt/wy

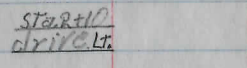
→ Spk W side 18" W. Ch. ↑ N side Hertel drive
→ = 30' N of rd. culv't outlet
→ H_2O level at rd culvt (1.5' conv)
→ F.L. outlet " "
→ top H_2O at pond outlet
→ = inlet pipe
→ F.L. outlet pipe
→ = ±300' E. of Road Culvert.

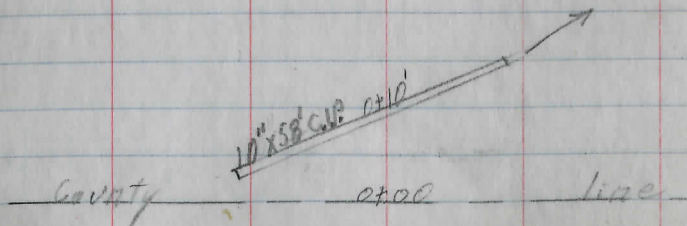
Topography

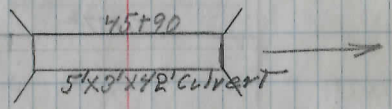

18+45
15"X42' Culvt.

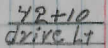

9+48
drive Rt

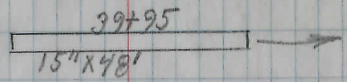

6+32
5'X3'X40' Culvt.


Start+10
drive Lt.

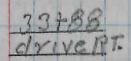

10"X58' C.M. 0+10
County
0+00
Line

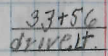

45+90
5'X3'X42' Culvert

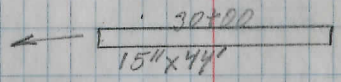

42+10
drive Lt

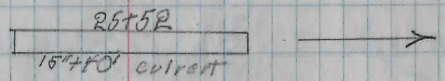

39+95
15"X48'

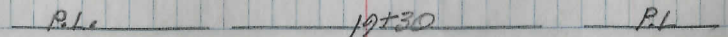

P.I.
38+80
P.I.


33+88
drive Rt.


33+56
drive Lt.


30+00
15"X44'


25+52
15"+50' culvert


P.I.
19+30
P.I.

Topography

81+37.2

17'

81+07.2

P.L. 77+41 P.L.

77+16
drive Rt.

68+66

15"x44' culvert

60+00
drive Lt.

℄ (TR 195) 12"x18.5' C.M.P. 58+09 (Barholomew)

98+46.9

P.L. 96+89 P.L.

95+51

15"x40'

93+00
drive Rt.

91+47
drive Rt.

83+16.8

10"x21.2 culvert

Topography

116+90
drive Rt.

109+73
drive Lt.

℄ cassels Cors. 109+07 Rd.
(TR 186 Taylor May)

107+84
15" x 40'

105+91
drive Lt.

99+60 — P.t.

99+44
drive Rt.

137+09
15" x 40' culvert

P.t. — 127+65 — P.t.

127+50
drive Rt.

127+30
15" x 36' culvert

122+96
15" x 38' culvert

118+60
15" x 34' culvert

Topography

U.S.R. 422 — 145+10 62

144+50
drive Lt. drive Rt.

142+80
drive Lt.

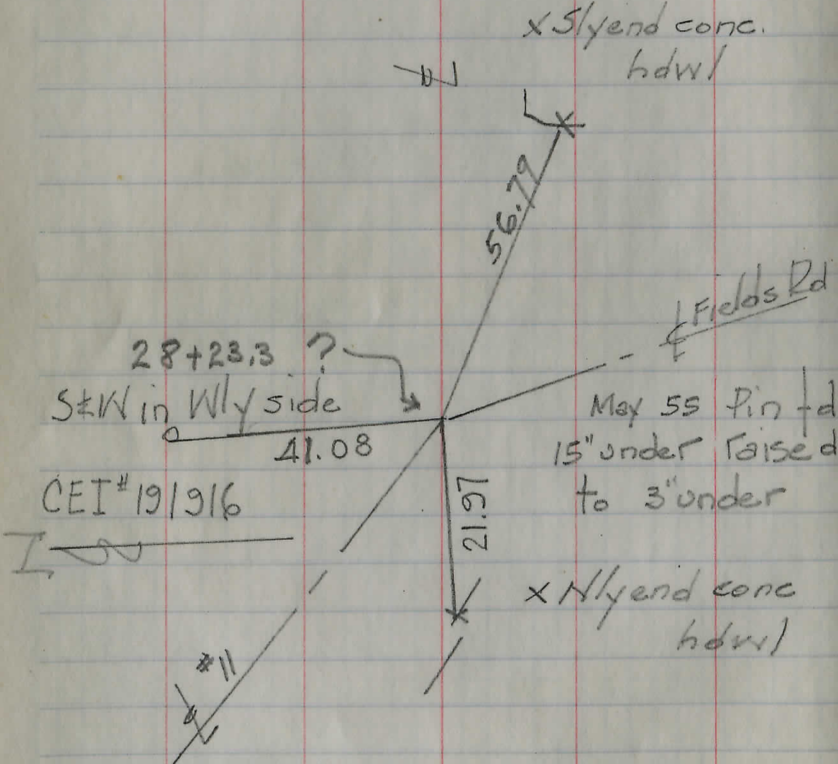
142+70
drive Rt.

142+30 — — — Pile

141x70
drive Rt.

141+15 — — — Pile

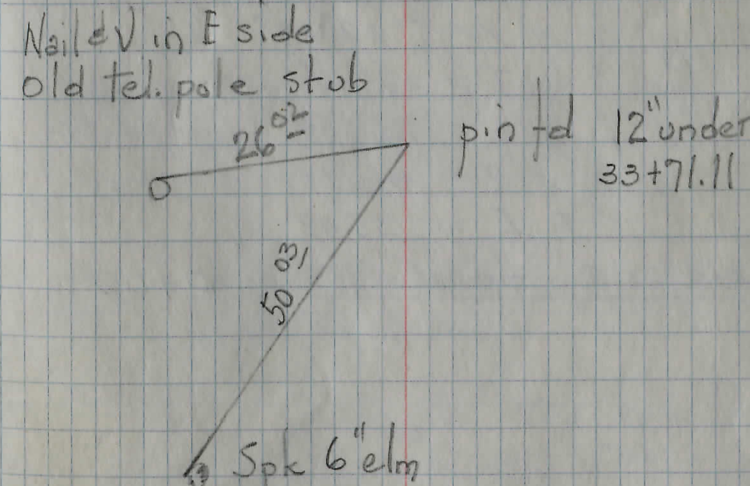
140+19
drive Lt.



May '55
Section 1 in Cuy Co
16' B.T. on water bd?
38' ditch - ditch

0+20 = end exist pav't

Bridge = 20' rdwy



Bainbridge Road - C.H. 11

Solon Auburn Road Sections A, B, C & D

WPSO Project 1011-A

1937.

P.T. Sta. 2+51.54 PT of Curve

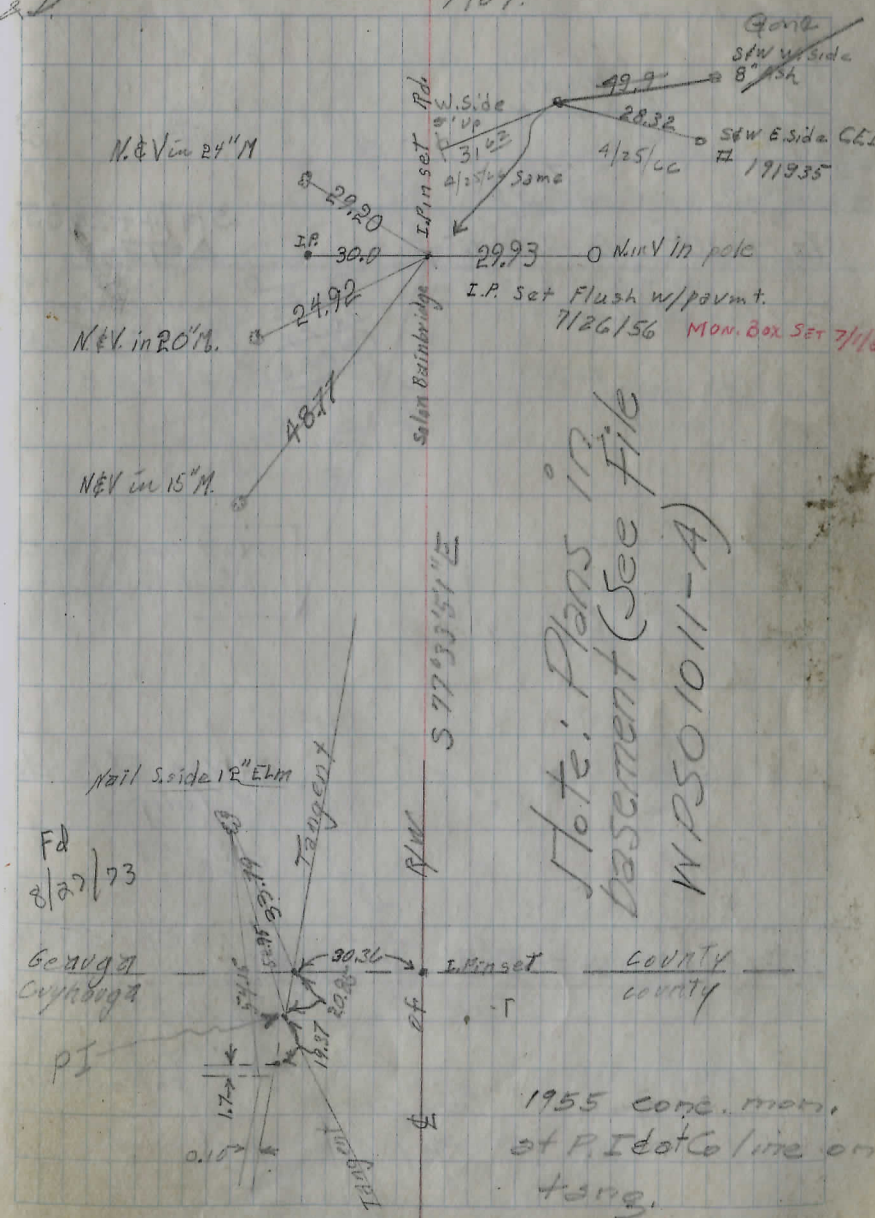
Note: These notes copied From State Highway Dept. Field bk:.

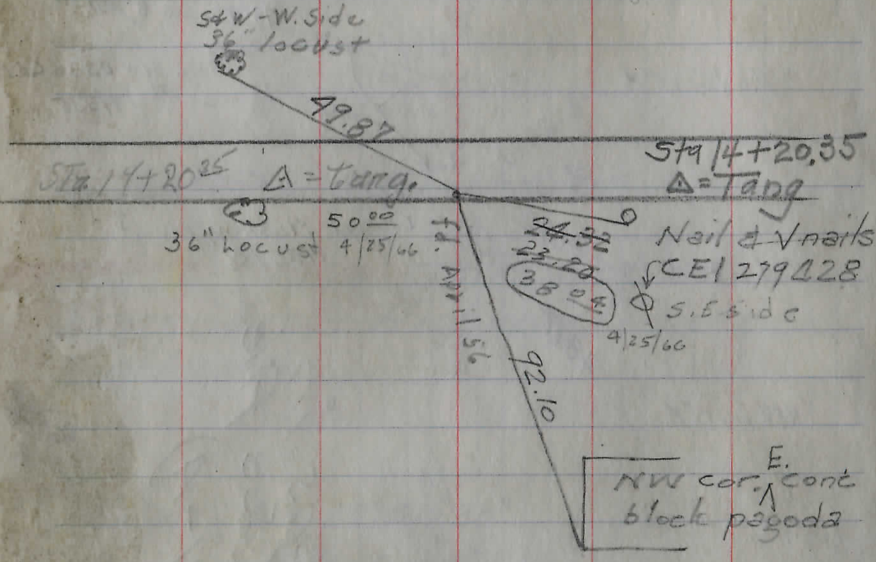
Total $\Delta = 29°08'30"$

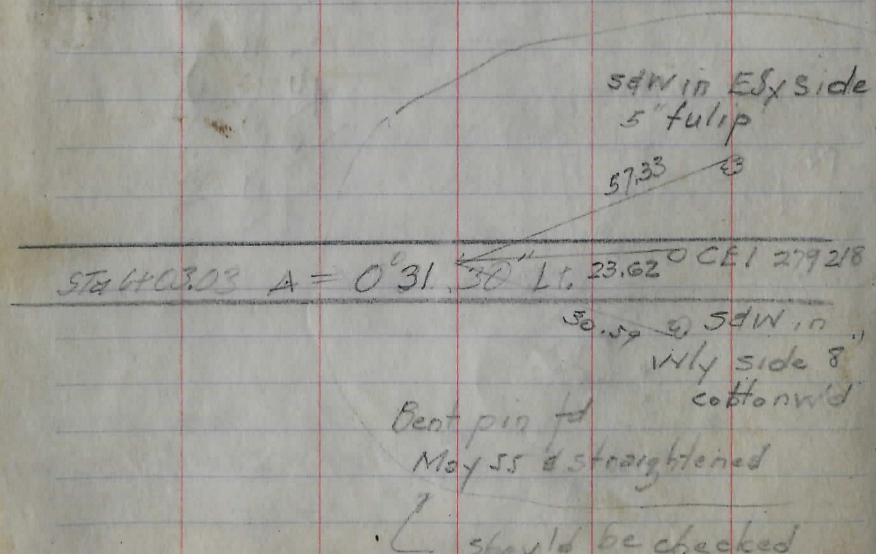
Curve Data.

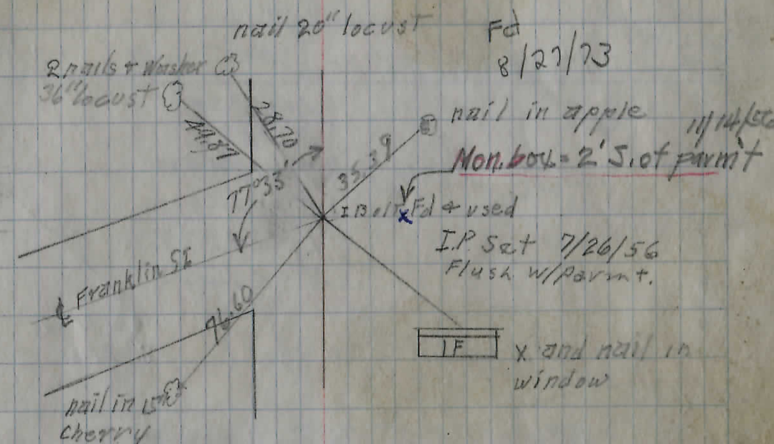
- $\Delta = 13°30'58"$ (in Geauga Co)
- $D = 5°22'24"$
- $T = 277.17$
- $L = 25.154$ Geauga County
- $R = 1066.28$
- $\mathcal{E} E = 35.43$

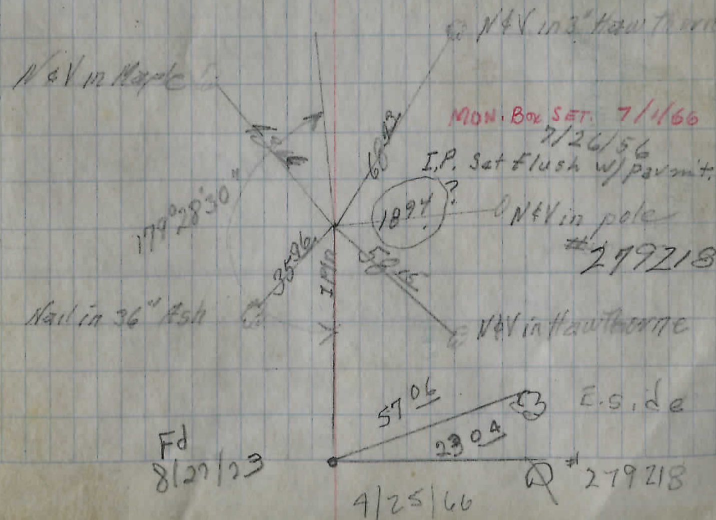
Sta. 0+00 Beginning of Project 0+00




S&W - W. side
36" locust
49.87
Sta 14+20.35
Δ = Tang.
Sta 14+20.35
Δ = Tang
36" Locust
50.00
4/25/66
fd. April 56
24.32
23.20
38.04
Nail & V nails
CEI 279228
S.E. side
4/25/66
92.10
NW cor. E. conc block pagoda


S&W in ESly side
5" tulip
57.33
Sta 6+03.03 Δ = 0°31' 30" Lt.
23.62
CEI 279218
50.59
S&W in
Wly side 8"
cottonw'd
Bent pin fd
May 55 & straightened
should be checked

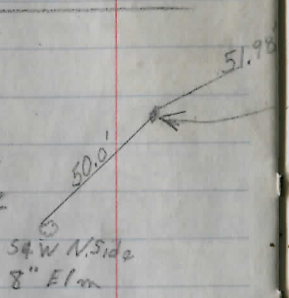

nail 20" locust
Fd
8/27/73
2 nails & washer
36" locust
44.87
28.70
77°35'
35.39
nail in apple
11/14/56
Mon. box - 2' S. of pavm't
I.B. Fd & used
I.P. Set 7/26/56
Flush w/pavm't.
Franklin St.
16.60
nail in 15" cherry
I F
X and nail in window


N&V in 8" Hawthorne
N&V in Maple
MON. BOX SET 7/1/66
7/26/56
I.P. Set flush w/pavm't.
179°28'30"
1894?
N&V in pole
#279218
35.96
Nail in 36" Ash
N&V in Hawthorne
57.06
23.04
E. side
Fd
8/27/73
4/25/66
#279218

Equation 34+92.52 back = 34+25.63 forward = -3.11

Sta. 23+71.44 Δ = 22°08' Rt.

Curve Data
- Δ = 22°08'
- D = 9°
- T = 124.52
- E = 12.66
- L = 245.93
- R = 636.62



Equation 28+73.10 back = 28+79.73 forward = -6.62

Sta. 28+23.21 Δ = 47°48' Lt.

28+23.21
56.42
79.73

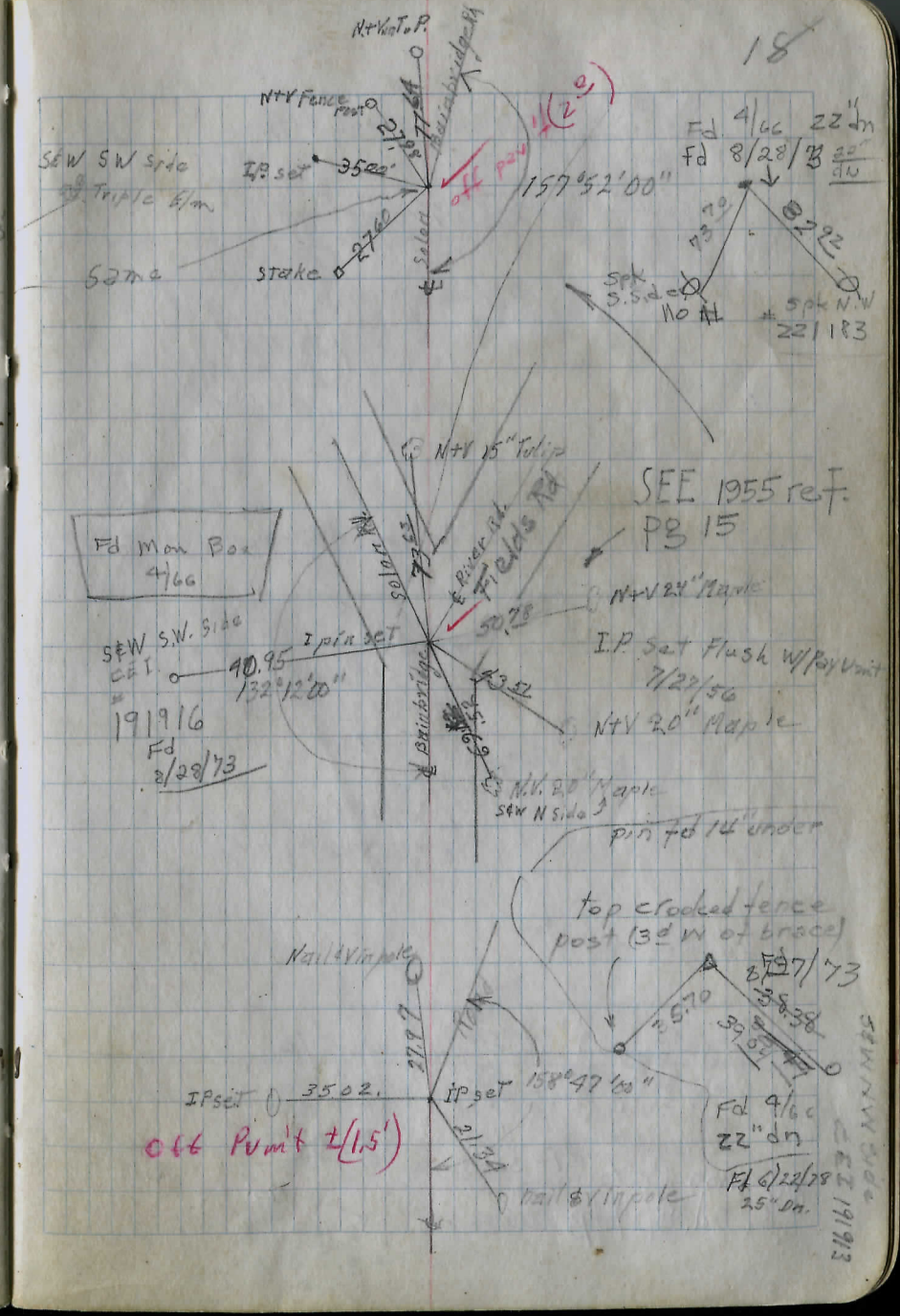
Curve Data
- Δ = 47°48'
- D = 45°
- T = 56.42
- E = 11.94
- L = 106.22
- R = 127.32

2873.31
56.42
2766.89

Equation 23+45.00 back = 23+47.29 forward = -2.74'

Sta. RR+28.50 Δ = 21°13'00" Lt.

Curve Data
- Δ = 21°13'00"
- D = 9°00"
- T = 119.24
- E = 11.69
- L = 235.74
- R = 636.62



Equation 54+77.34 back = 54+80.83 forward = − 3.49

59?

Sta. 53+51.69 Δ = 25° 17' Base Line

Curve Data — Construction ℄

- Δ = 25°17'
- D = 12°
- T = 107.09
- E = 11.87
- L = 210.69
- R = 477.47

PI = 53+73.74

Equation Sta 48+32.25 back = 48+32.12 forward = − 0.17

Sta. 41+23.45 Δ = 5° 28' 45" Lt.

Curve Data

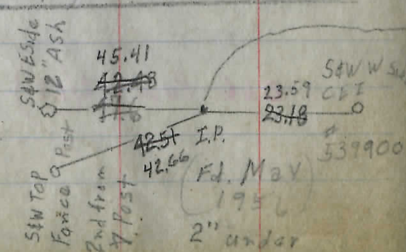
- Δ = 5°28'45"
- D = 2°30'
- T = 109.64
- E = 2.61
- L = 219.16
- R = 2291.83

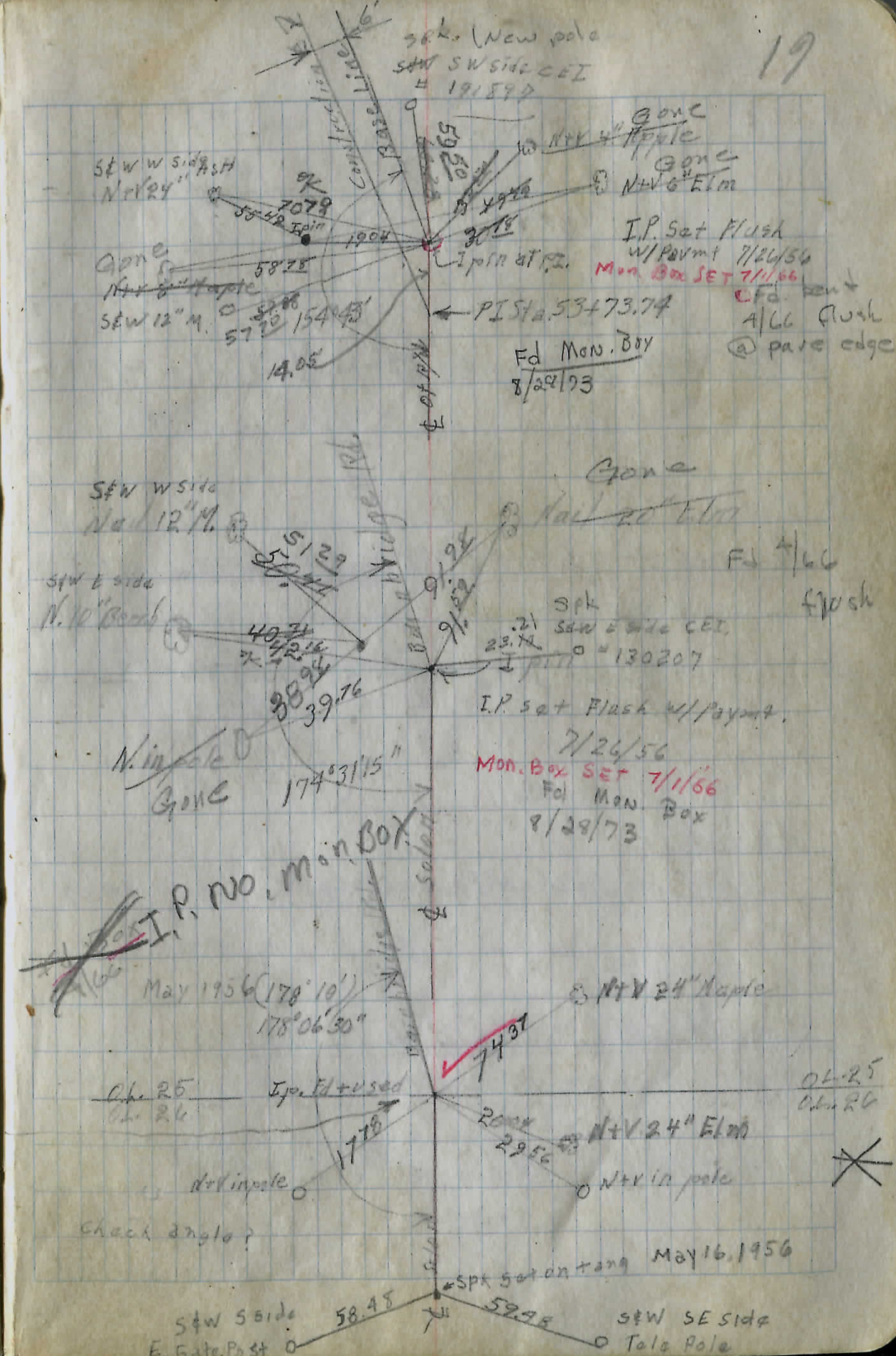
Sta 42+16.50 1°59' 30" def. Lt.

53

D. Wetzel
D. King
ref checked 5/13/71
to reset Mon Box
No Mon. Box.
I.P. Fd. 8/27/73

I.P. Set Flush w/Pavmt. 7/26/56





Equation =
PT = Sta 64+33.29 back = 64+34.52 forward = −1.23

Sta. 61+50.21 $\Delta = 11°15'42"$ Base Line

Curve Data Construction ℄

$\Delta = 10°27'42"$
$D = 2°30'$
$T = 209.82$
$E = 9.62$
$L = 418.41$
$R = 2291.83$

PI = 62+24.70

Equation
PC = Sta 60+19.25 back = 60+19.87 forward = +0.07

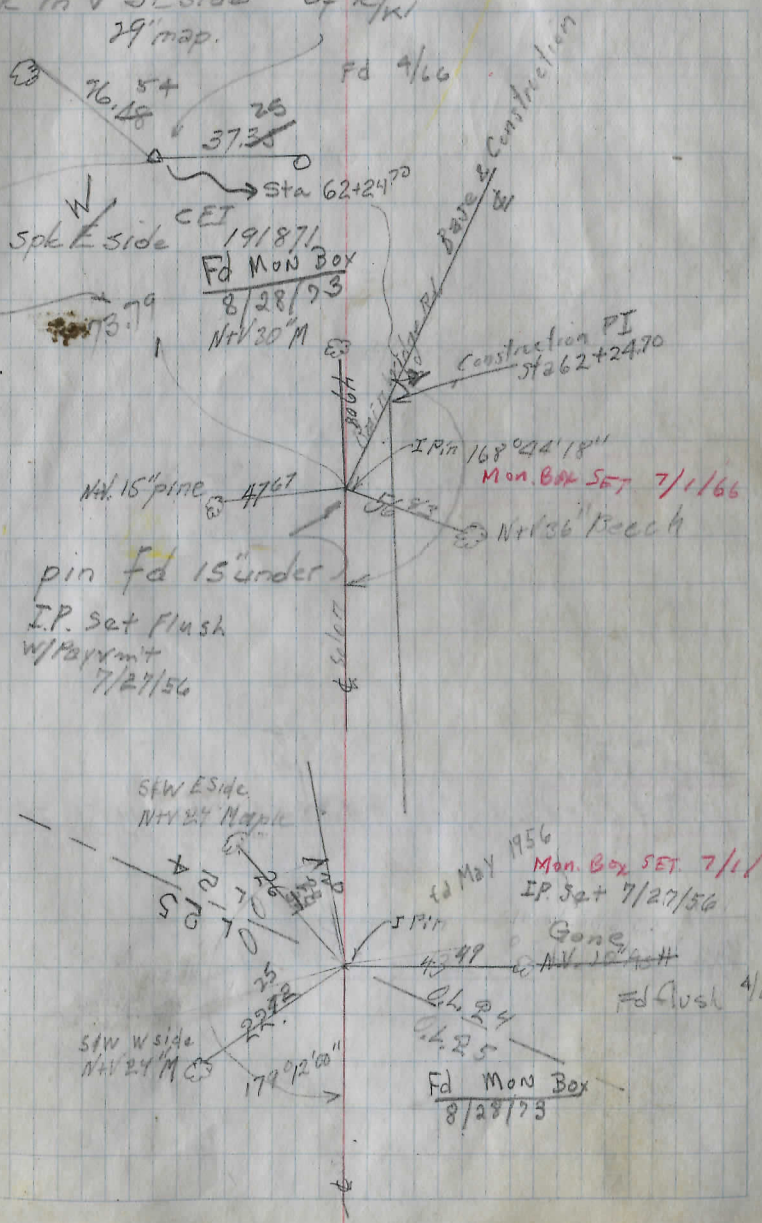
Sta. 56+20.96 $0°48'$ def. Lt. Base Line

No angle in Construction Line.

Construction Line is Tangent from 53+59.59 to
62+24.30

20

Bent pin fd at ℄ P.I.
Spk in ∨ SE side of R/W
29" map.



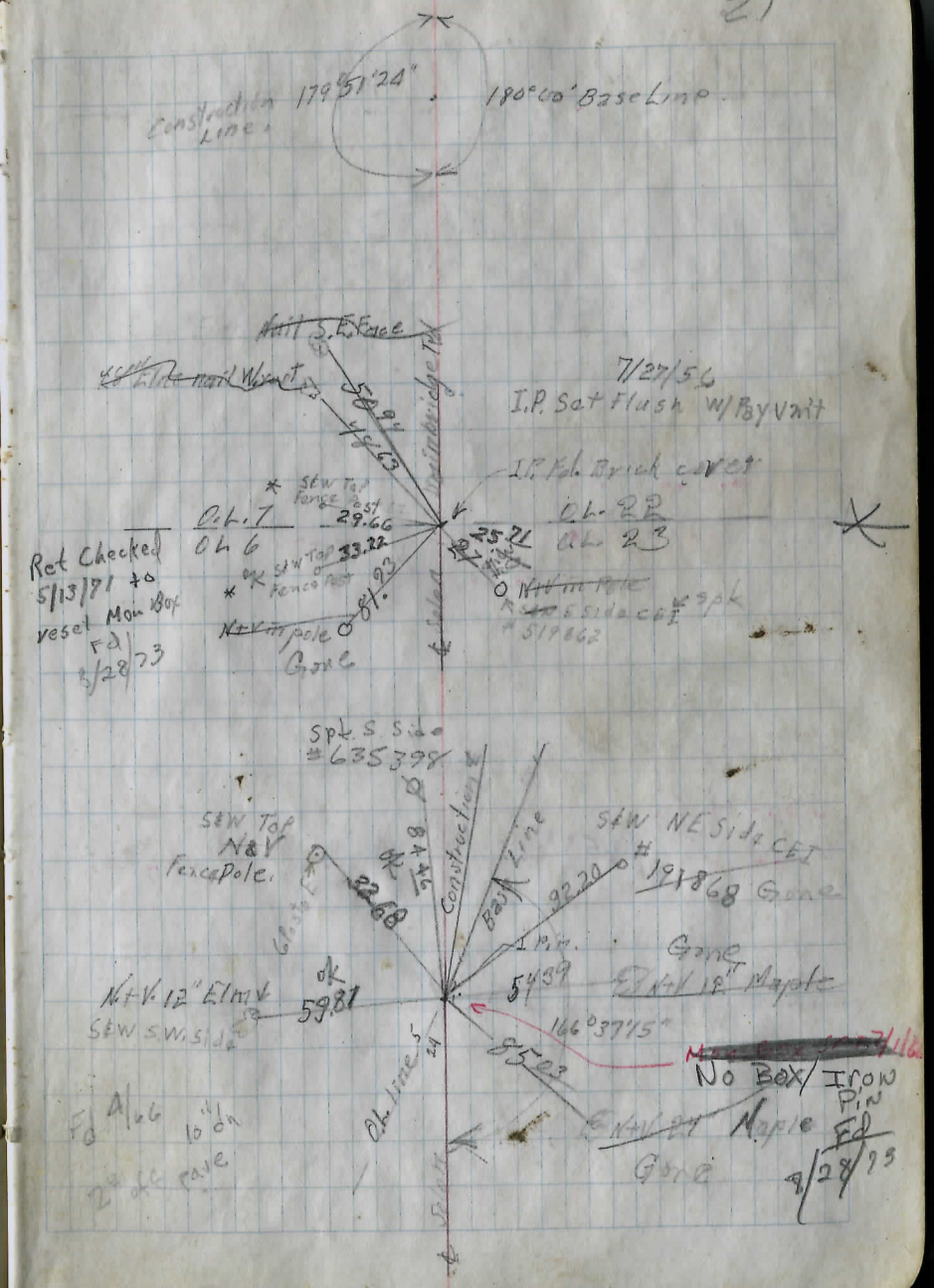
Sta 96+60 Δ = 0°08'36" Lt. Construction Line
0°00' Base Line

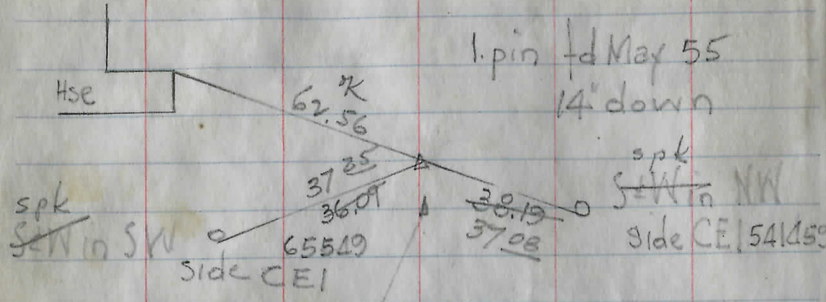
Equation =
= 84+05.62 Back Sta. 8570 Forward temp.
Equation = -94.31

Equation =
PT = 68+82.62 back = 68+84.33 forward = -1.71'

Sta. 66+65.62 Δ = 13°22'45" → Base &
13°04'21" → Construction

Curve Data Construction ℄ {Δ = 13°04'21", D = 3°, T = 218.73, E = 12.51, L = 435.75, R = 1909.86'}



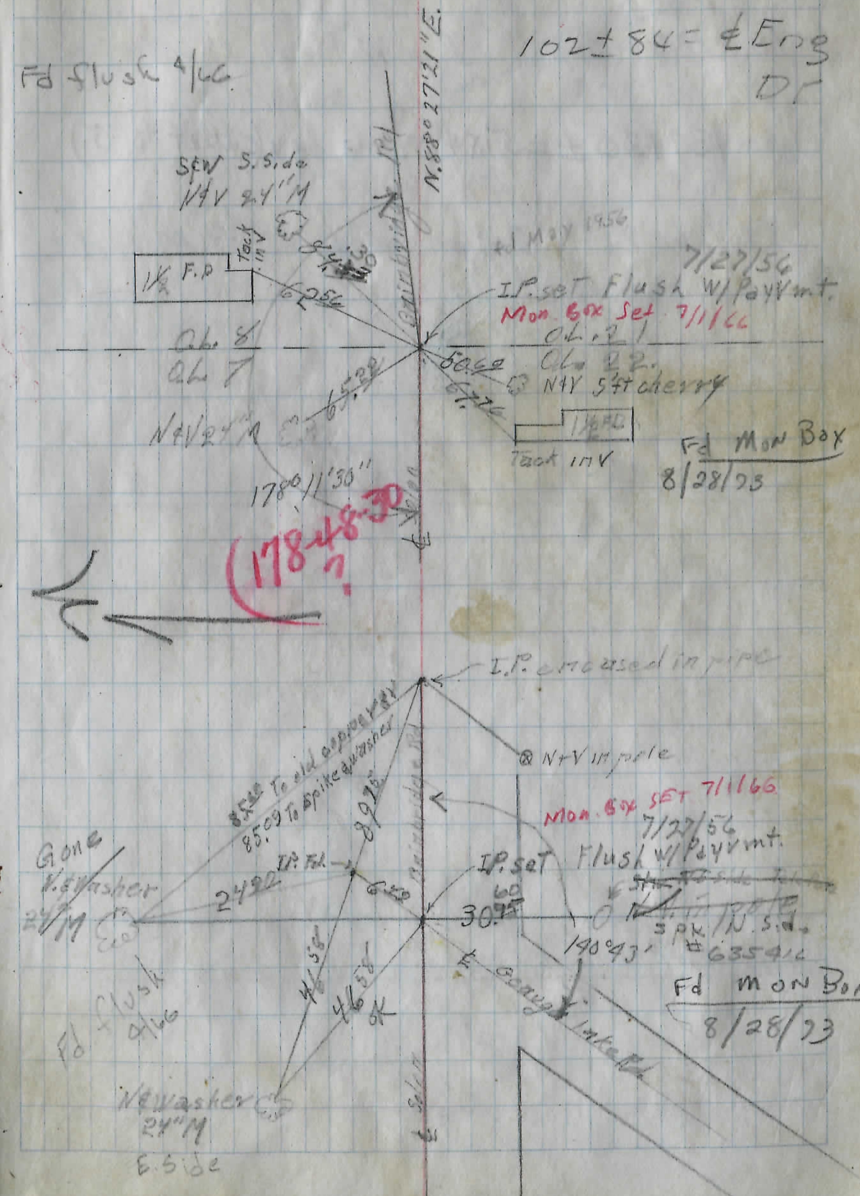


Sta. 97+29.43 1°11'30" defl. Lt.

Sta. 97+97.43 POT

97.65

Sta. 97+02.78 POT



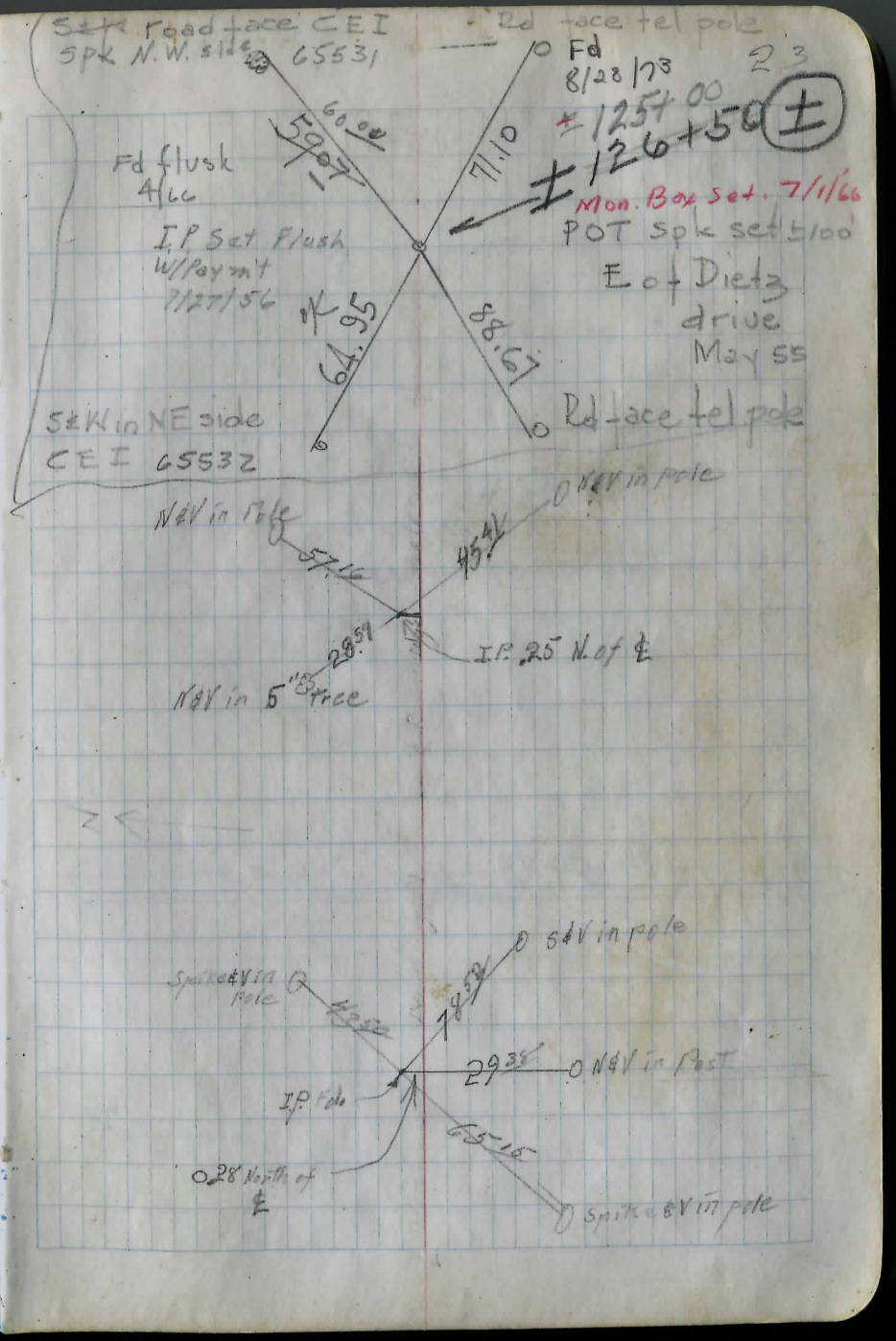
Sta 133+31.56 I. pipe found 28.65' North ℄

130+30 ± = 5'X4' stone hoy (outlet to 5)

Sta 126+73.66 I.P. pc found 28.40 ft. North of ℄

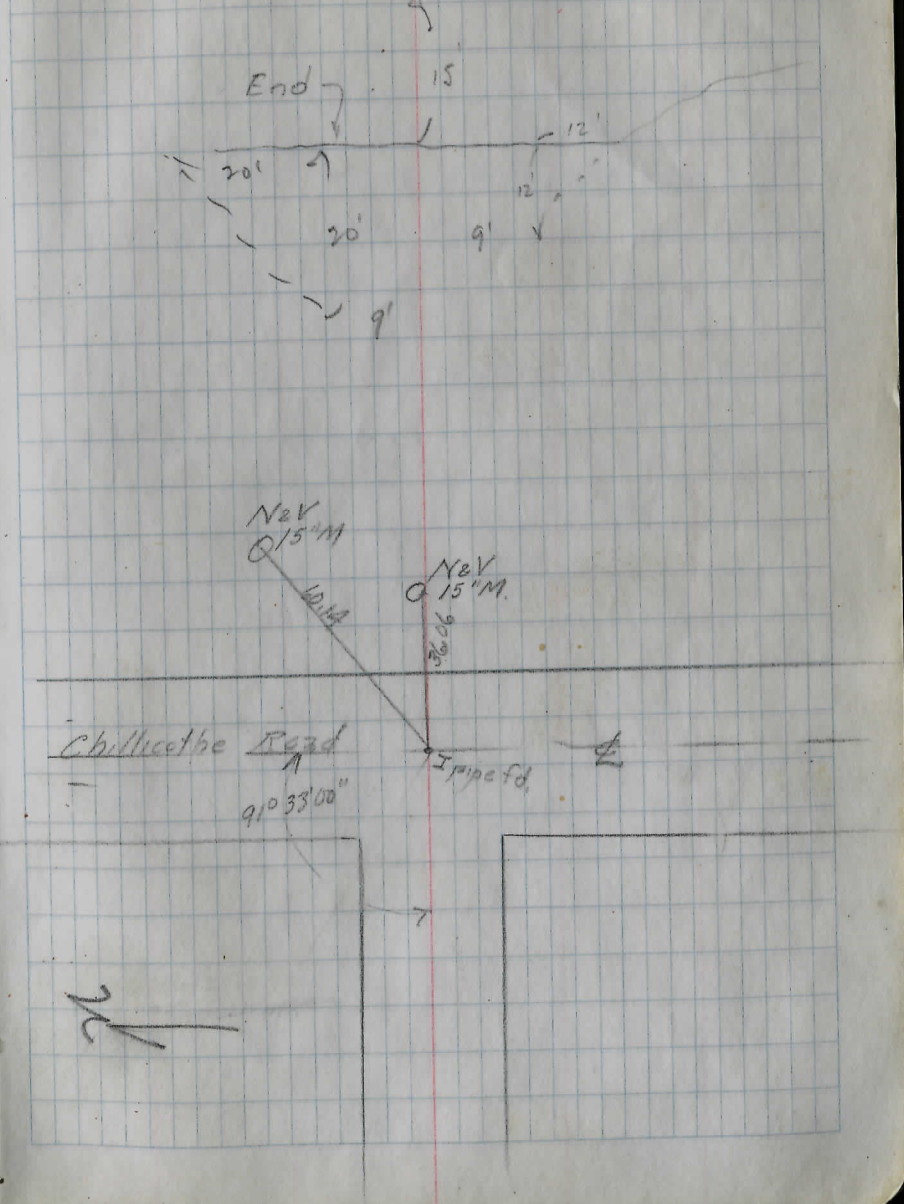
Sta. 116+89.27 Tang. POT

Sta. 113+96.09 Tang. P.O.T.



147+59.70
+ 13.31 Equations
146 44.59 Net Length = 2.773 miles

Sta 147+59.70 End of Project

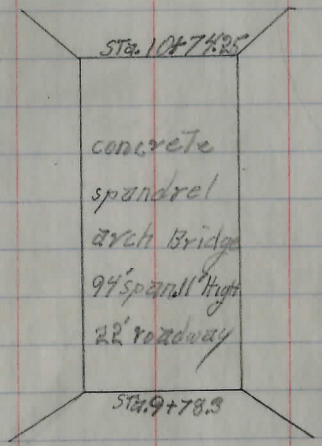


Bench Marks

B.M. No.	description
	Government B.M. aluminium tablet Top H.W.
B.M.# 1	× Top step first house W. of Ctr. S. side of road
B.M.# 2	× on cor. conc. foundation sec. house W. of Ctr. S. side of Rd.
B.M.# 3	× on S. Headwall culvert
B.M.# 4	Two nails in Pole No. 2913
B.M.# 5	× N. Headwall stone culvert.
B.M.# 6	nail in root 18"M N. side of road at inter. George Lore Rd.
B.M.# 7	2 nails in root 50" Elm.
B.M.#	2 nails in pole N. side opp. pole # 2954
B.M.# 10	nail in root 24"M. N. side road
B.M.# 11	nail in side of pole # 2969
B.M.# 12	nail in side of pole # 2916
B.M.# 13	nail in side of pole # 2981
B.M.# 14	Top nail root 24"M. opp F.C. Jackson ent.
B.M.# 15	nail root 24"M. S. side of road
B.M.# 16	nail in side of pole # 2997
B.M.# 17	nail in root 24"M.
B.M.# 18	× in N.W. abut. Bridge
B.M.# 19	nail in side pole S. side

Sta.	Elevation
Bissells P.O.	1166.410
	1166.615
	1144.516
131+43.5	1135.044
119+79	1120.024
110+13.39	1100.914
97+-	1117.800
86+32	1031.556
66+92	1025.833
61+0	1041.135
52+-	1024.882
41+99	1018.936
35+60	1010.242
	953.831
25+60	922.357
16+87	912.131
12+00	910.204
9+78	909.149
2+51	935.582

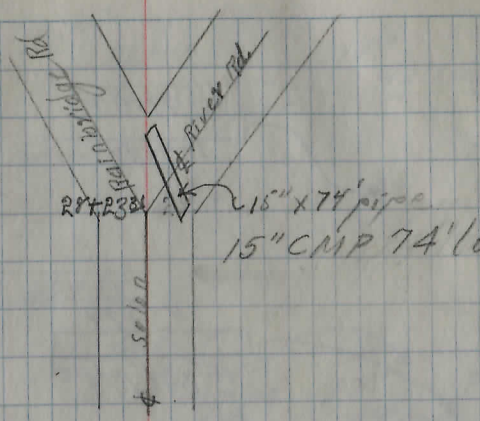
Topography



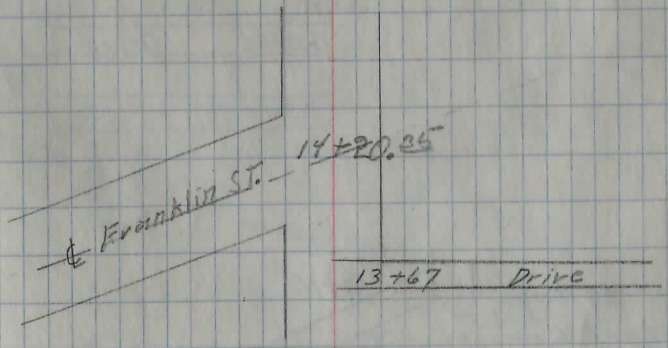
Drive 9+28 9+36 Drive

Drive 3+60

County C+00 line



21+19 Drive



49+00 — 15" Pipe 44' long.
15"X44' pipe

43+79 — 15" pipe 39'16 long.
15"X39' pipe

42+16.57 — Ch. 25 / Ch. 26

Prop. Line. C.L 25 / Ch. 26

33+52 Drive

15" CMP 24' long extended with 16' new pipe total length 48'

31+10
15"X24' C.M.P

72+41 — 15" Pipe 42' long
15"X42' Cul. pipe.

Ch. 6 / Ch. 5 — 69+70 ± — Ch. 23 / Ch. 24

Drive 66+75

66+68
15"X49' Cul. pipe 15" Pipe 49' long

Drive 62+49

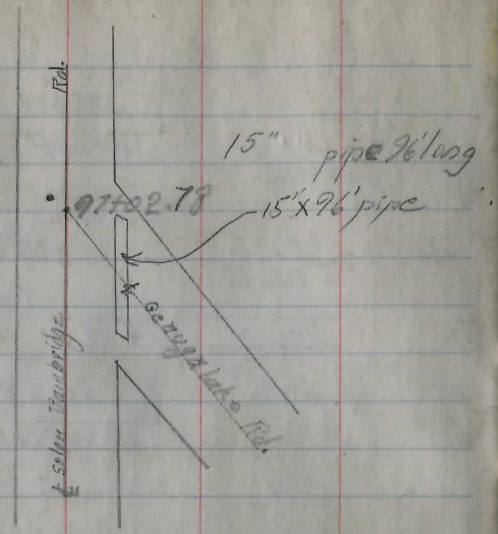
Center line of Culv. 57+42

Drive 56+43

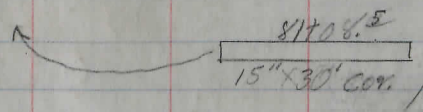
Prop Line C.L. 24 / Ch. 25

56+20.96
C.L. 24 / Ch. 25

53+00
15"X48' pipe 15" Pipe 48' long.



Ch. 7 — 94+05.6 End. — Ch. 22
Ch. 6 — 85+00 Back — Ch. 23



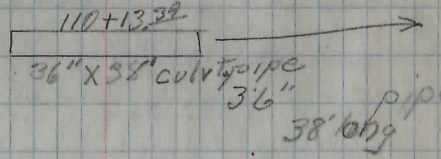
15" CMP pipe 24' long extended with 15' new pipe total length 39'

Drive 78+59

77+44 Drive

Ch. 9 — 113+96.03 — Ch. 20
Ch. 8 — Ch. 7.1

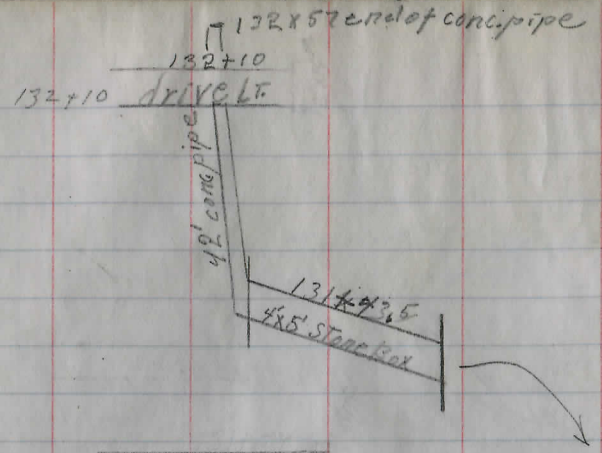
111+80 Drive



Drive 101+00

99+65 Drive

Ch. 8 — 94+29.43 — Ch. 21
Ch. 7 — Ch. 22



Drive 131+04

130+67 P.L.

P.L. 126+73.66

Drive 125+59

125+29 Drive

Drive 122+42

Drive 145+67

144+82 Drive

143+95 P.L.

P.L. 141+00

Drive 137+90

136+60 P.L.

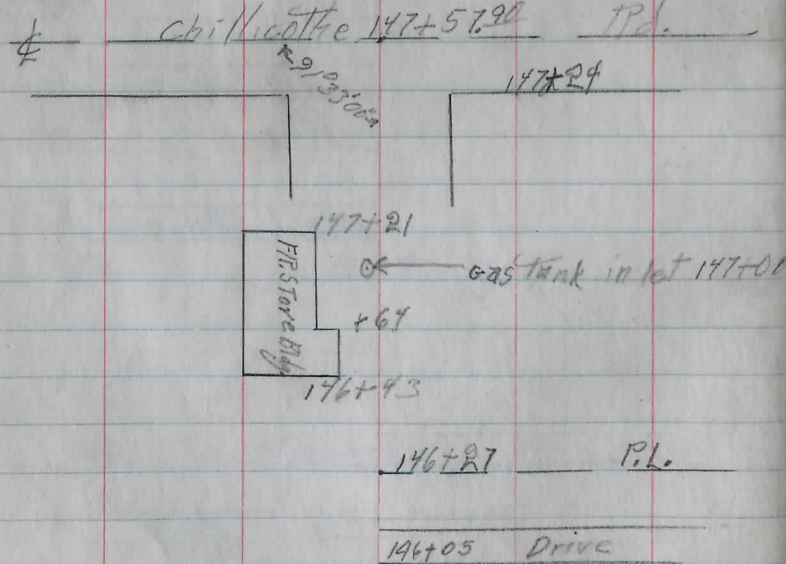
136+19 Drive

135+95 P.L.

134+68 Drive

P.L. 133+31.56 P.L.

133+26 Drive


℄
Chillicothe 147+57.90 Rd.
91°33'00"
147+24
147+21
F.R. Store Bldg
gas tank in lot 147+01
+64
146+43
146+27 P.L.
146+05 Drive

5-10-43
Pom Bundles

Almy Ditch Auburn

B.M.	1.77	101.77		100.00	Ass.
F.L. (West)	12" drive crock		8.15	93.62	
0+0 = E side Almy drive					
1+0				94.67	
2+0				94.37	
3+0				93.87	
4+0				93.37	
T.P.	4.23	99.67	6.33	95.44	
5				93.0	
6				92.9	
7				92.5	
8				92.0	
9				91.3	
	2.89	96.03	6.53	93.14	
10				90.6	
BM			4.06	91.97	
11				90.0	

Spike SE root 20" Pine 75' S.E. of Almy's house

Stk	Ch.
5.67	7.1
6.30	7.4
5.63	7.9
6.33	8.4
3.52	6.7
4.21	6.8
5.46	7.2
5.21	7.7
6.53	8.4
3.90	5.4

SE root 50" Oak 10+50 25' W of channel

4.50 6.0

96.03

12				
13				89.53
T.P.	7.33	101.12	2.24	93.79
B.M.			1.08	100.04

F.L. (West) drive crock 8.76
F.L. (N) 12" Conc. 7.26
Culvt (250' to 300' apart

See Next Pg for Final grades

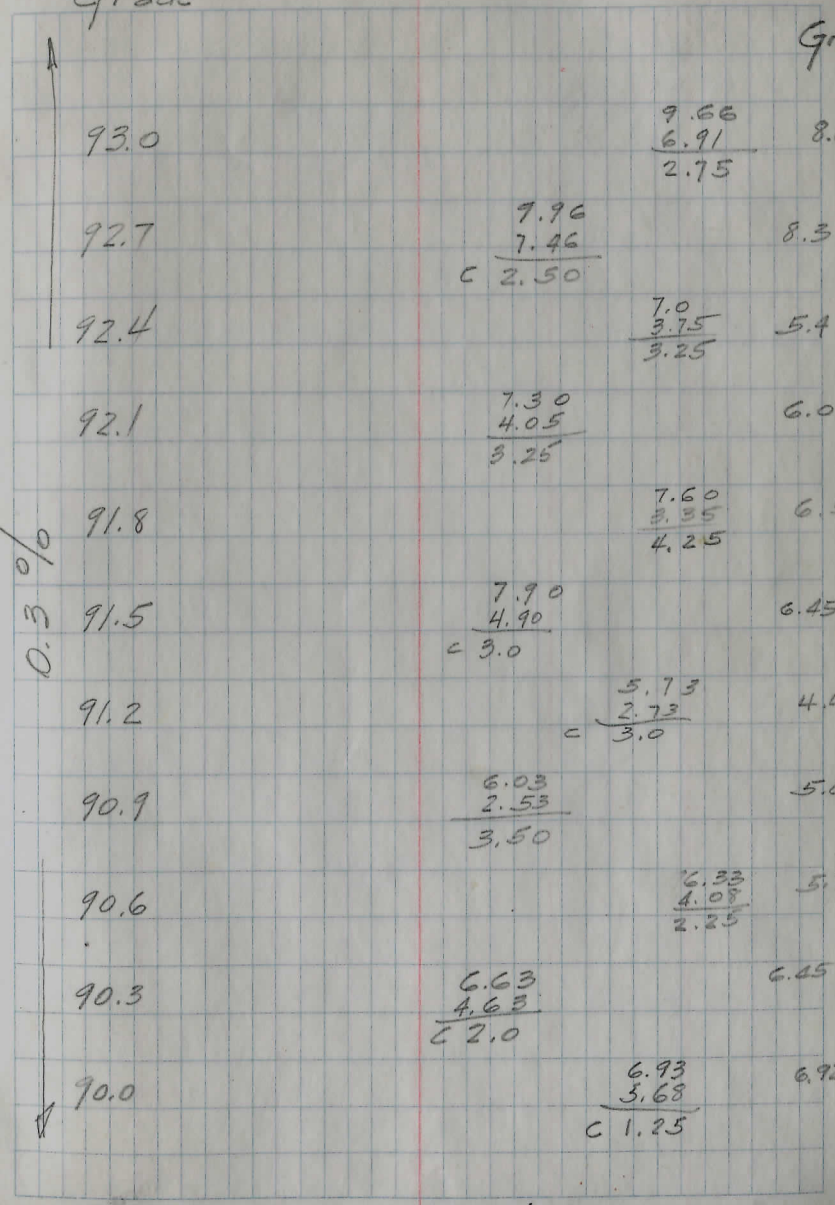
stk ch 35

5.04	6.3
5.46	6.5

5-13-43
Tom Hall
Randles
10:30 - 12:00

	+		−		
BM.			2.60	100.06	100.00
1					
2					
T.P	7.02	102.66	3.76	95.64	
3					
4					
5					
6					
T.P.	5.22	99.40	2.75	94.18	
7					
8					
9					
10					
11					
BM.	4.96	96.93		91.97	

Final grade Almy ditch

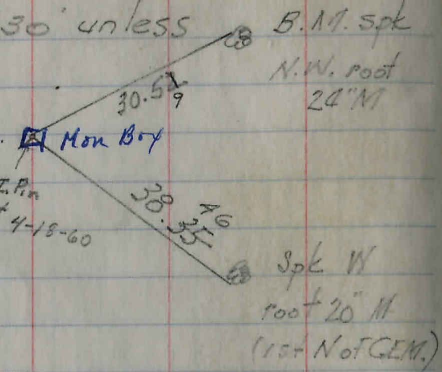


10/21/50
Maynard
Pomeroy
Ford

AUBURN ROAD
CH#4 D

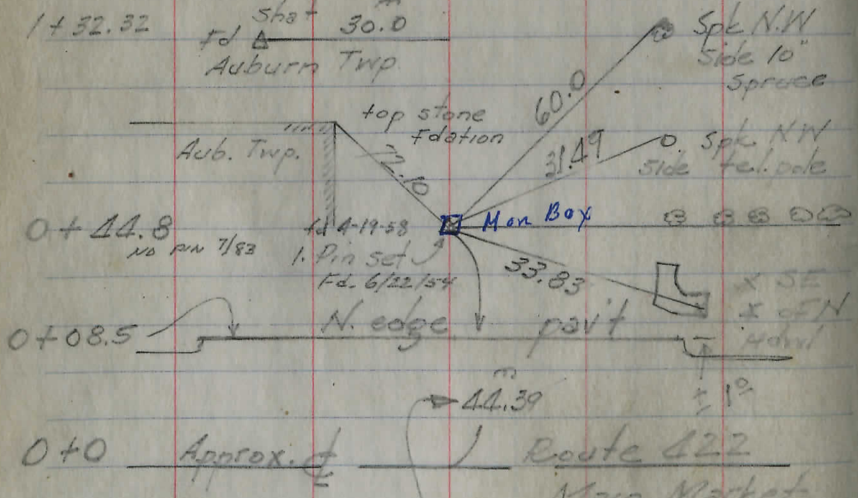
Staked at 30' unless otherwise noted

5+0 P.O.T. spk set
Fd. 6/22/54
4-19-58
F.O. 3/4 IP 7/83

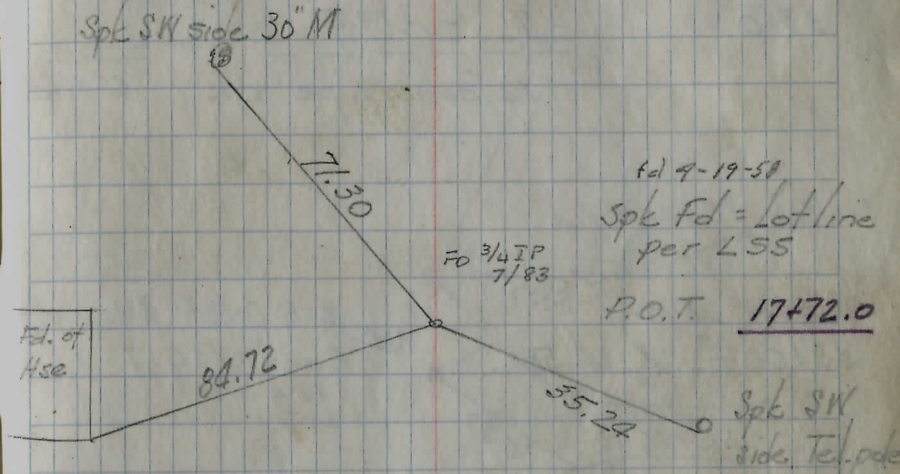


3+66.6 I.P. Fd. 29.78
Shatford

1+32.32 Fd Shat 30.0
Auburn Twp



Actual ℄ per Aub.
Cem. survey 1954 field bk #176 pg. 22

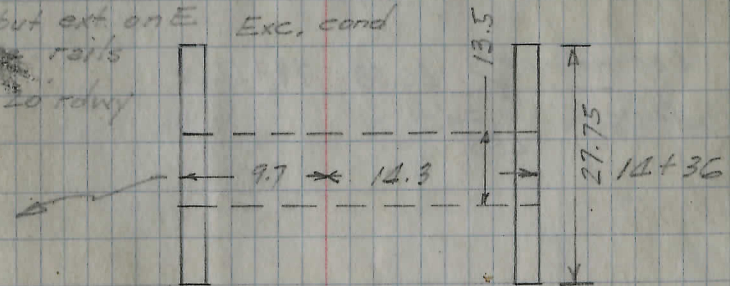


fd 4-19-58
Spk Fd = Lotline
per LSS

P.O.T. 17+72.0

Conc slab culvt (bridge?)
Stone abuts W and 8' conc
abut ext on E. Exc. cond
pipe rails
± 20' rdwy

Ht = ±6.5



I.P. Fd 21.18 9+00.2

43+0 25' □ stk

±8'

39+0 9 19.5

12" conc. pipe ok 6" tile

Spk NE side 46" Pipe

64.5

BM Spk E root 24" M

30+00 05 26.58

Mon Box Fd. ¾ IP 7/83

I.P. set P.O.T

fd. 4-19-58 OK '73"

38.30

DRIVE

Spk SE side 26" M

Bartholmew Dines I.P. Fd LSS 30.58 28+56.2

11.6

20+99.7 14.8

12" C.I.P. OK 12" Corr

39

Spk SE side 30" Ash

75.62

P.C 53+63.70 Spk set

Mon Box No IP 7/83

87.7

Spk NE root 24" Elm

Cut 4 9" C.I.P. Pipe OK

12' 16'

50+98

4" tile

43+77

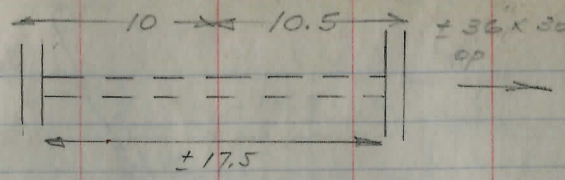
6.8 18.1

18" conc. pipe OK

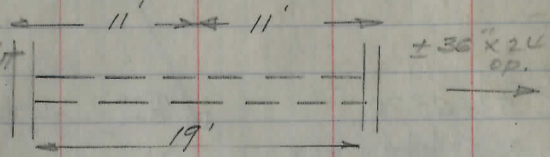
43+76

8" Field Drain

Stone & conc culvt NE



66 +75.5



61+37.3 Stone & conc culvt poor

Δ = 16-16-40 LT
D = 3-00
R = 1909.86
T = 273.13
L = 542.59
E = 17.43

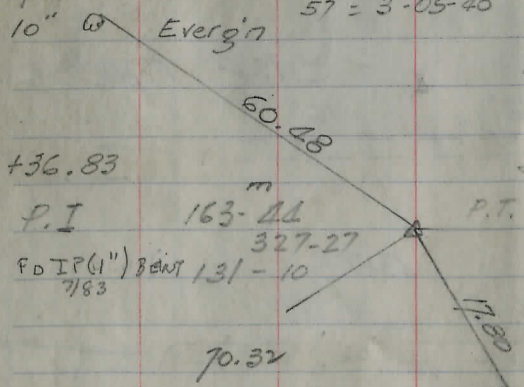
P.C 53+63.70
P.T 59+06.31

36.28	54+0	0-32-40
	+50	1-17-40
	55+0	2-02-40
	+50	2-47-40
	56+0	3-32-40
	+50	4-17-40
	57+0	5-02-40
	+50	5-47-40
	58+0	6-32-40
	+50	7-17-40
	59+0	8-02-40
P.T. +06.79		8-08-20

59+0 = 0-5-40
+50 =
58 = 1-35-40

+50 =
57 = 3-05-40

Spk NE side
10" Evergn



56+36.83
P.I
163-44
327-27
FD IP(1") BENT 7/83
131-10

Spk NE side 5" W.Ch

Spk N side 9" Evergn

40

80+68

12" Corr. I.P. Fair
± 19' Rdwy

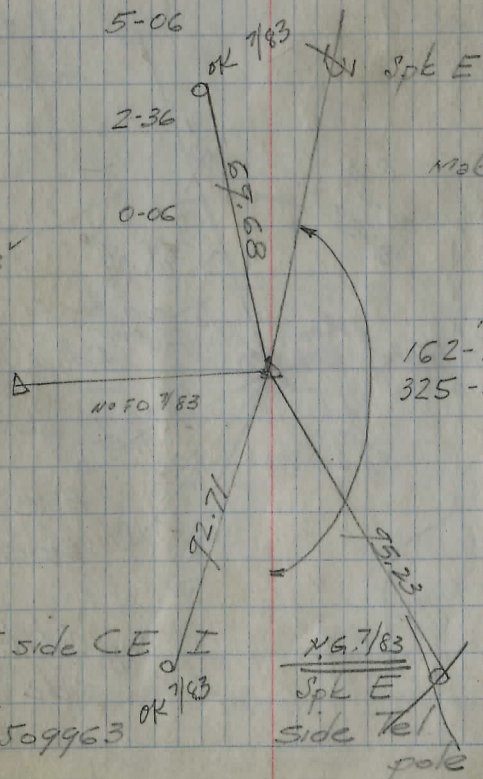
76+00

10.7
12.7

6" c.i.p. nearly plugged
8-34 Replace with 12"

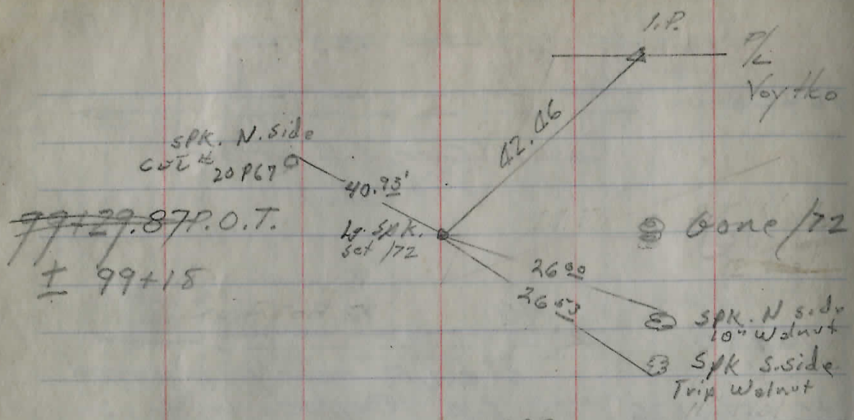
P.C 67+61.26
68+0
+50
69+0
+50
70+0
+50
71+0
P.T +03.93

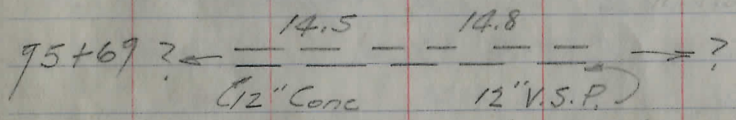
7-36 38.76
5-06
2-36
0-06

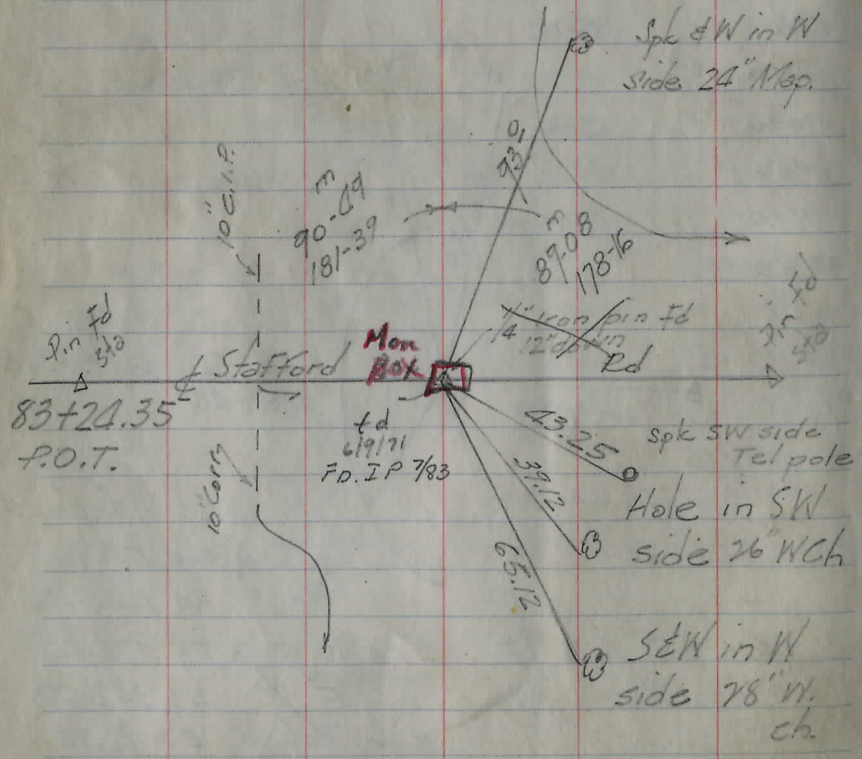


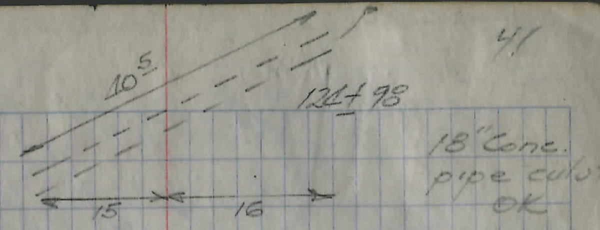
P.I.
162-52
325-44
69+33.88

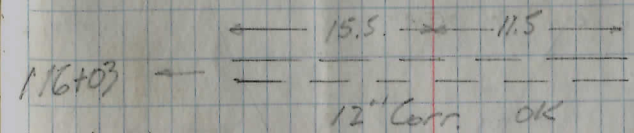
Δ = 17° 08' Rt.
D = 5°
R = 1145.92
T = 172.62
L = 342.67
E = 12.93

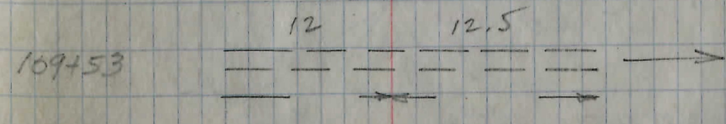






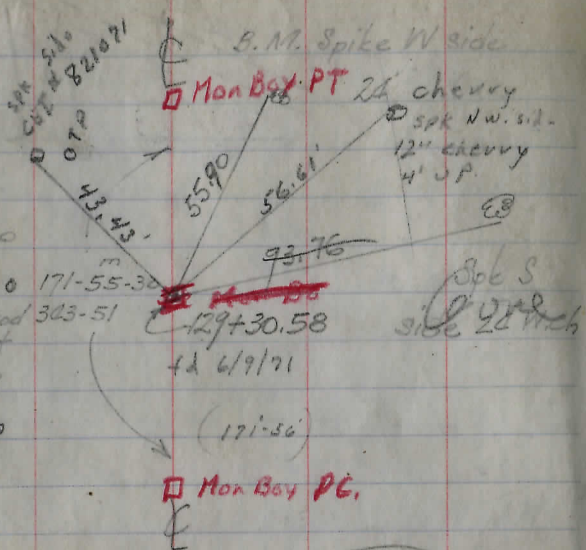






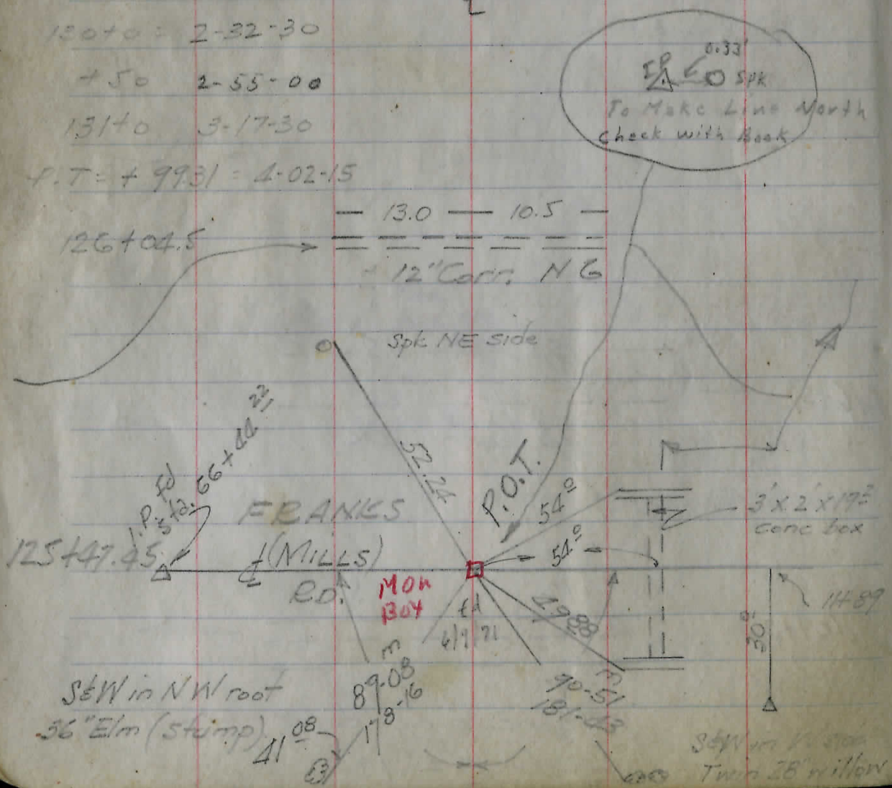
18" conc. pipe culvt OK
Edwy = 19'

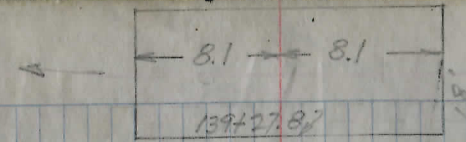
Δ = 8-04-30 L   Δ/2 = 4-02-15
D = 1-30
R = 3819.72
T = 269.60
L = 538.33
E = 9.5



P.C = 126+60.98

127+0 : 39.02	= 0-17-30	
+50	0-40-00	Reinf. rod set
128+0	1-02-30	
+50	1-25-00	
129+0	1-47-30	
+50	2-10-00	
130+0	2-32-30	
+50	2-55-00	
131+0	3-17-30	
P.T = +99.31	= 4-02-15	



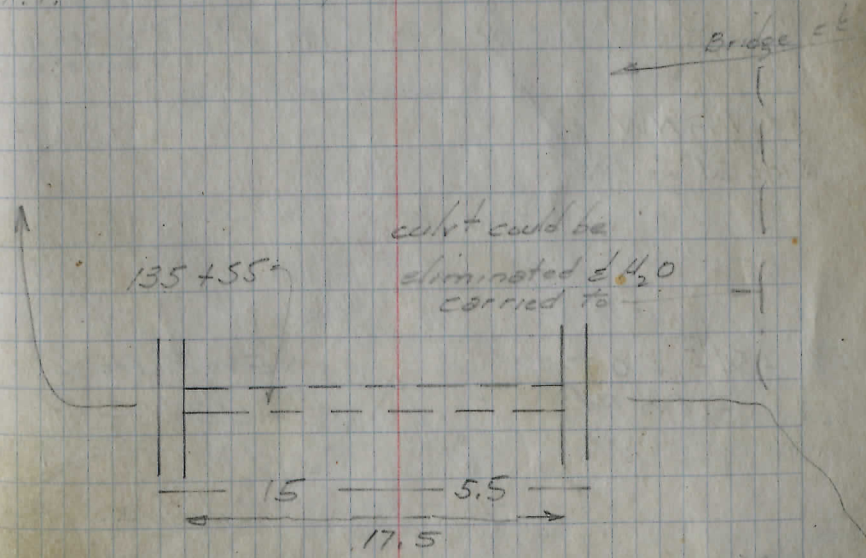


Δ = 6-17   Δ/2 = 3-09-30
D = 2°-30'
R = 2291.83
T = 126.46
L = 252.67

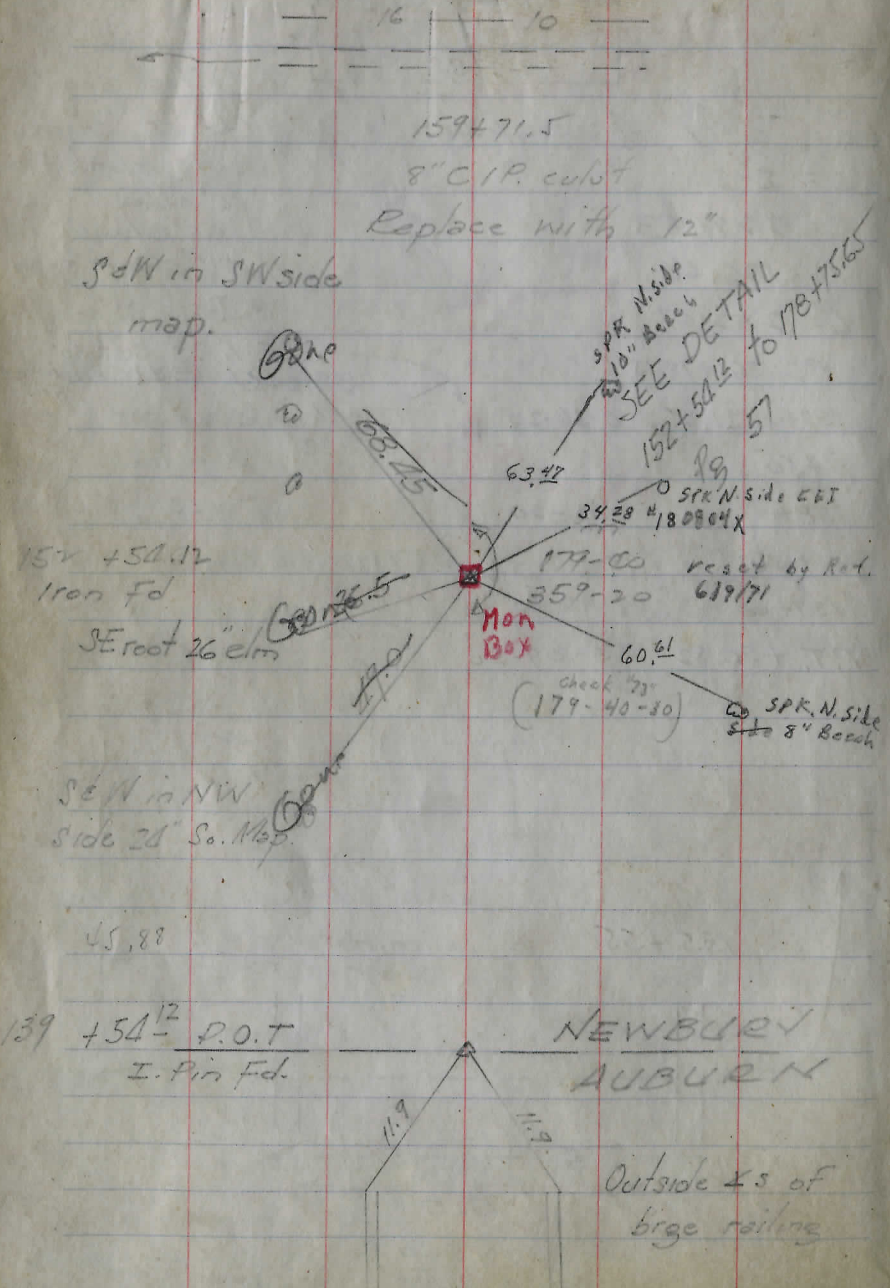
Steel pony truss, stone abuts, plank floor
16' plank
15.5' rdwy
15.5' clear span
8" I's @ 32" spcg

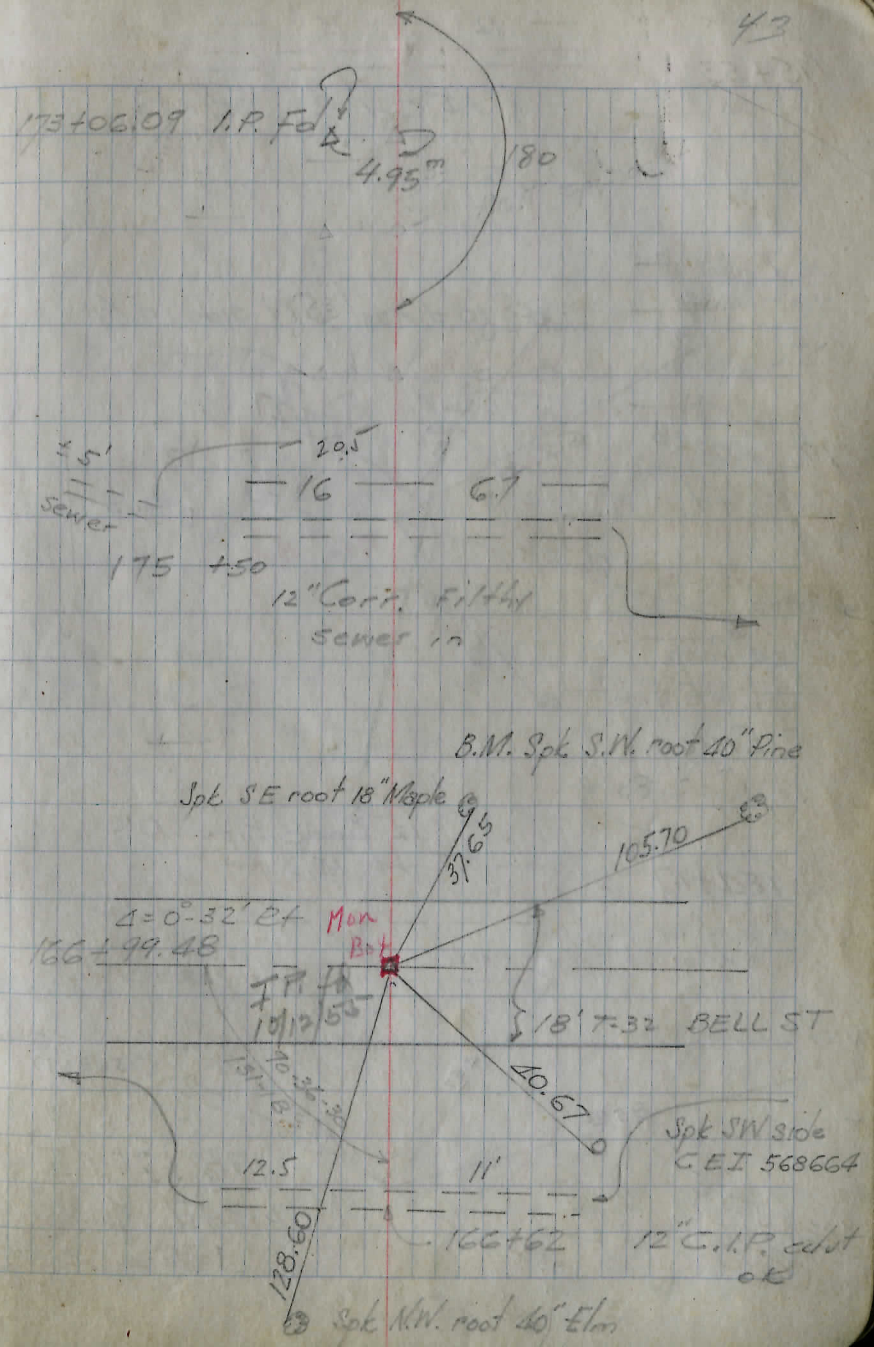
PC 136+78.15

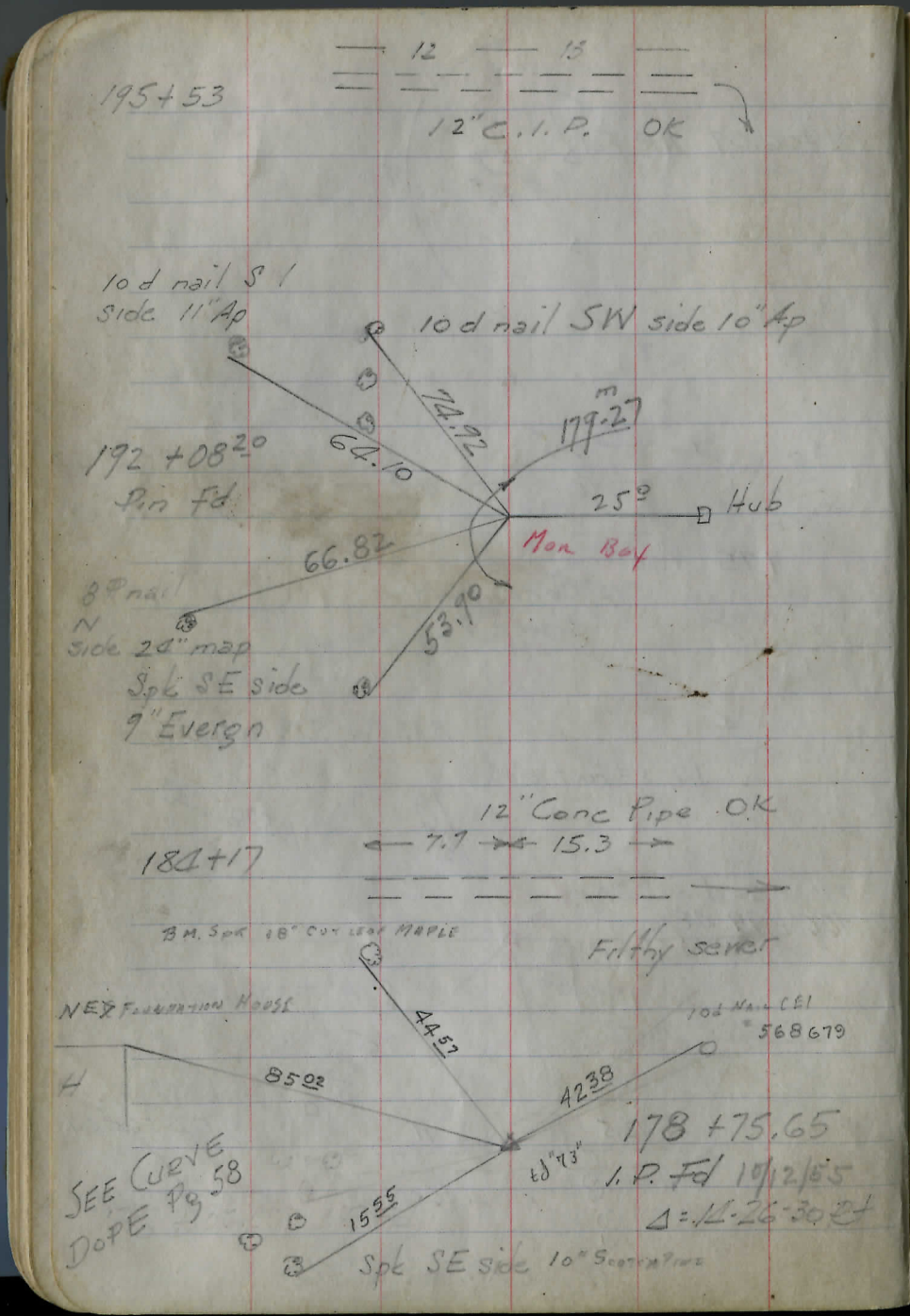
137+0 = 21.85	= 0-16-20	138+04.61 Mon Box	Ref. I.P.s set 30' E&W on bisect of Δ rod set
+50		173-41 / 347-22	± 9 Ext
138+0	1-31-20		± 12.3'
+50		(173-43)	173-45
139+0	2-46-20		
P.T. +30.82	3-09-30		



36" span x ± 20" ht. x stone culvt very poor cond. Eliminate


16
10
159+71.5
8" C.I.P. culvt
Replace with 12"
S&W in SW side
map.
Gone
SPK N. side 10" Beech
SEE DETAIL
152+54.12 to 178+75.65
Pg 57
68.45
63.47
34.28
SPK N. side CEI #180804X
152+54.12
Iron Fd
179-00
359-20
reset by Rol. 6/19/71
Gone 26.5
SE root 26" elm
Mon Box
60.61
Check '73
(179-40-30)
SPK. N. Side 8" Beech
S&W in NW side 24" So. Map.
45.88
139+54.12 P.O.T
I. Pin Fd.
NEWBURY
AUBURN
11.9
11.9
Outside ∠s of brdge railing


173+06.09 I.P. Fd.
4.95'
180
5'
Sewer
20.5
16
6.7
175+50
12" Corr. Filthy
sewer in
B.M. Spk. S.W. root 40" Pine
Spk. S E root 18" Maple
37.65
105.70
Δ=0°-32' Rt
Mon Box
166+99.48
I.P. Fd 10/12/55
18' T-32 BELL ST
40.67
Spk SW side CEI 568664
12.5
11'
166+62
12" C.I.P. culvt ok
128.60
Spk N.W. root 40" Elm


195+53
12
13
12" C.I.P. OK
10d nail S'l side 11" Ap
10d nail SW side 10" Ap
74.92
179.27
64.10
192 +08.20
Pin Fd
25°
Hub
Mon Boy
66.82
8d nail N side 28" map
53.90
Spk SE side 9" Evergn
12" Conc Pipe OK
181+17
7.7
15.3
B.M. Spk 18" Cut Leaf Maple
Filthy sewer
NE Foundation House
10d Nail CEI 568679
44.57
85.02
42.38
178 +75.65
I.P. Fd 10/12/65
Δ = 44-26-30 Rt
SEE CURVE DOPE Pg. 58
15.55
Spk SE side 10" Scarlet Pine

Spk S.W. side CEI 563709
166.29
43.93
I.P. Fd 5' under Spk set 1' under
221 +06.93
Mon Boy
℄ Music St.
12.10
Spk SE side 16" Catalpa
58.4
15-26-30
150.04
Spk N.E. root 16" Maple
77.08
Spk SW side 14" Locust
36" Conc. pipe
± 18' rdwy
14
14+
215+94.5
No find outlet
211+30
10.2
10.8
± 8" C.I.P.
uncovered by chief shovel operator J.M.
± 8" C.I.P.
no find outlet end
200+66
12.5
9'
15'
203+10
12" Conc. pipe
Big hump in ctr relay!

TOPOG No 4 DEF

—+— = Telpole —H— = Electric

12" Conc

+76 16'

26" M 18 +71

Small trees

+52

+50 27

4+45 28.5 28" M

Hedge

P/L H +69

CEM

3+40

2+97 31 12" M

2+83

2+54 27'

0+90 31' 8" Pine

shrub 20' 1+96 31' 10" M

31' 20" M

Topo taken on curves

0+0 ± M. M. Ed

US 222

9+25

9+02 26.5

21.5 8+07 31

10" Pine 26 +91

12" M 20.5 +67

30' +58 26.5

15" M 19 +38

15" M 19 7+08

10" Pine 18.5 +47

+31

27.5

To 1X 20'-30' map

29 +12

30" M 17.5 +10

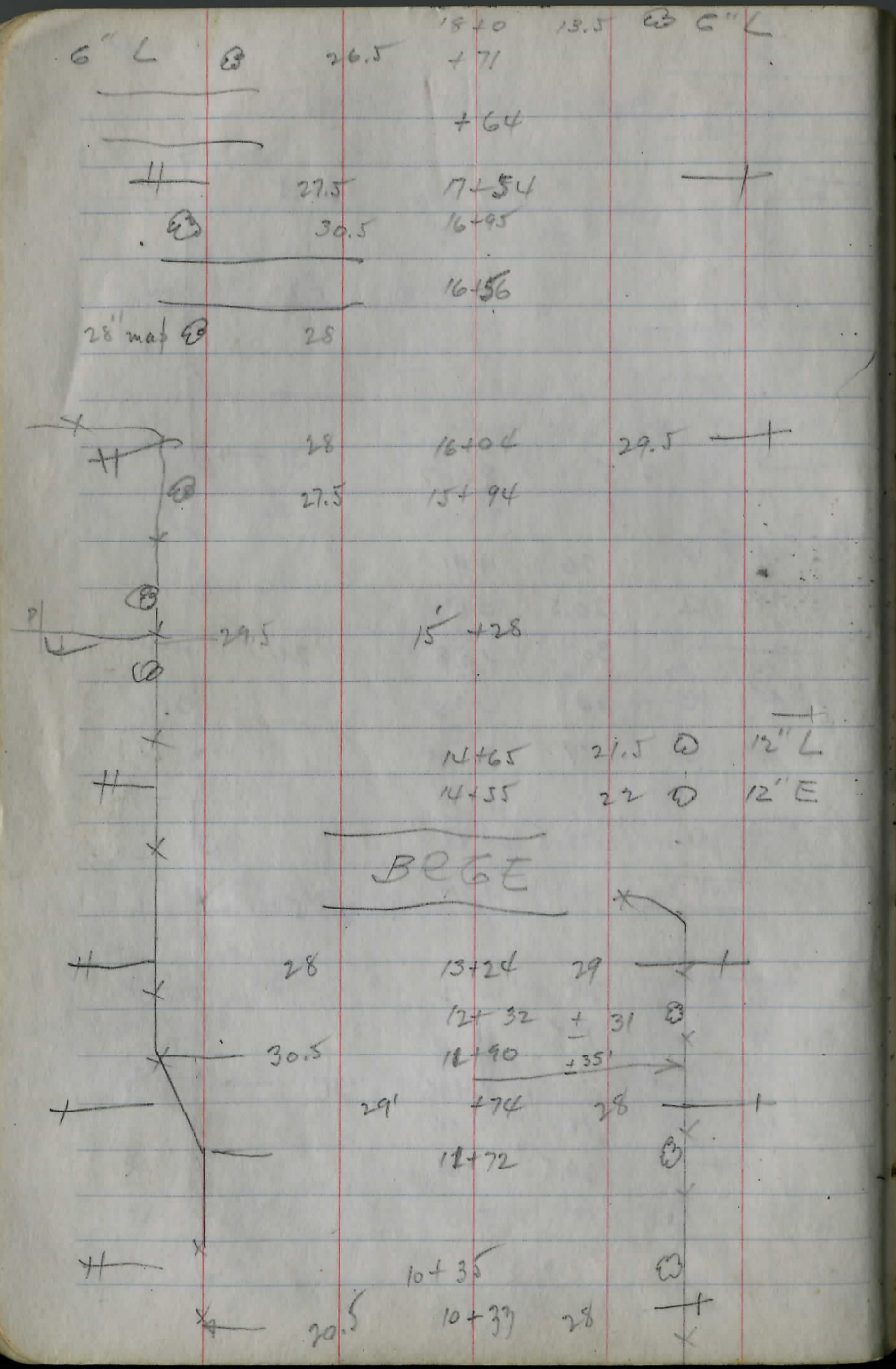
6+06 31'

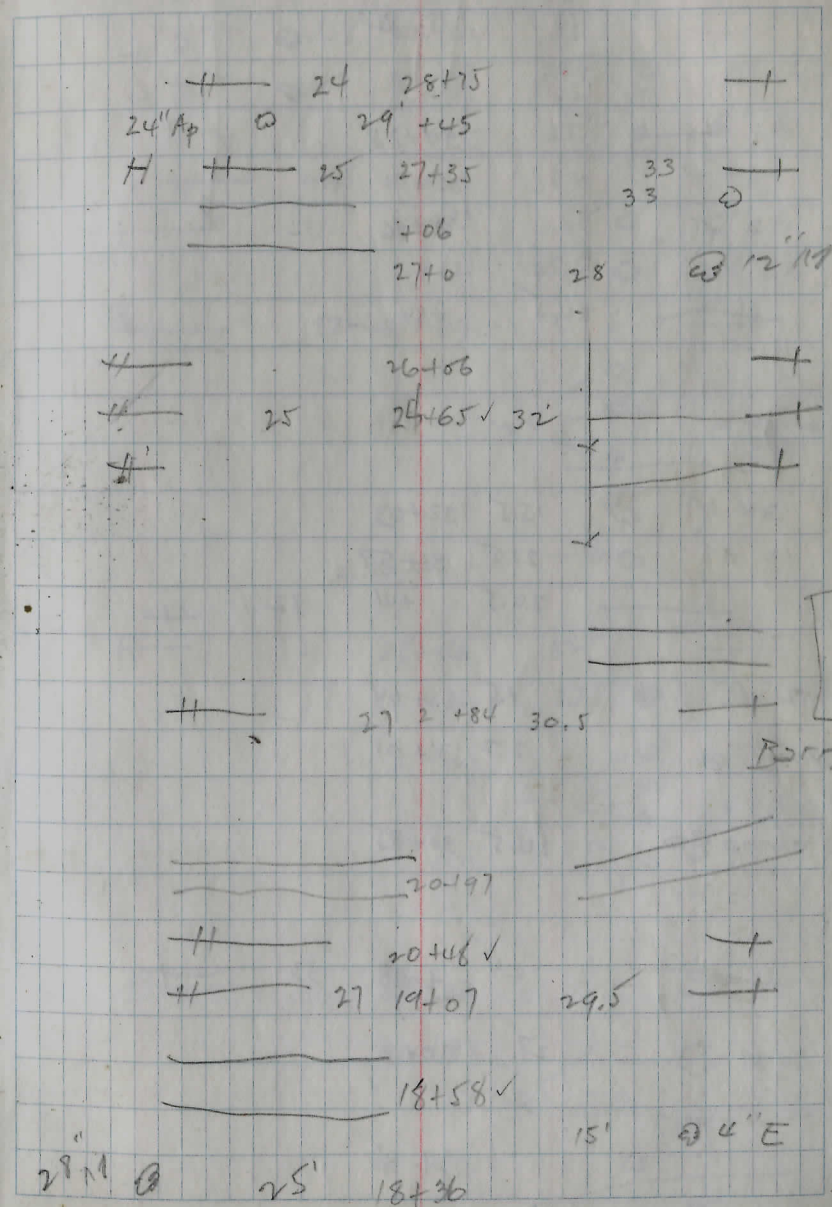
26" M 18 +54

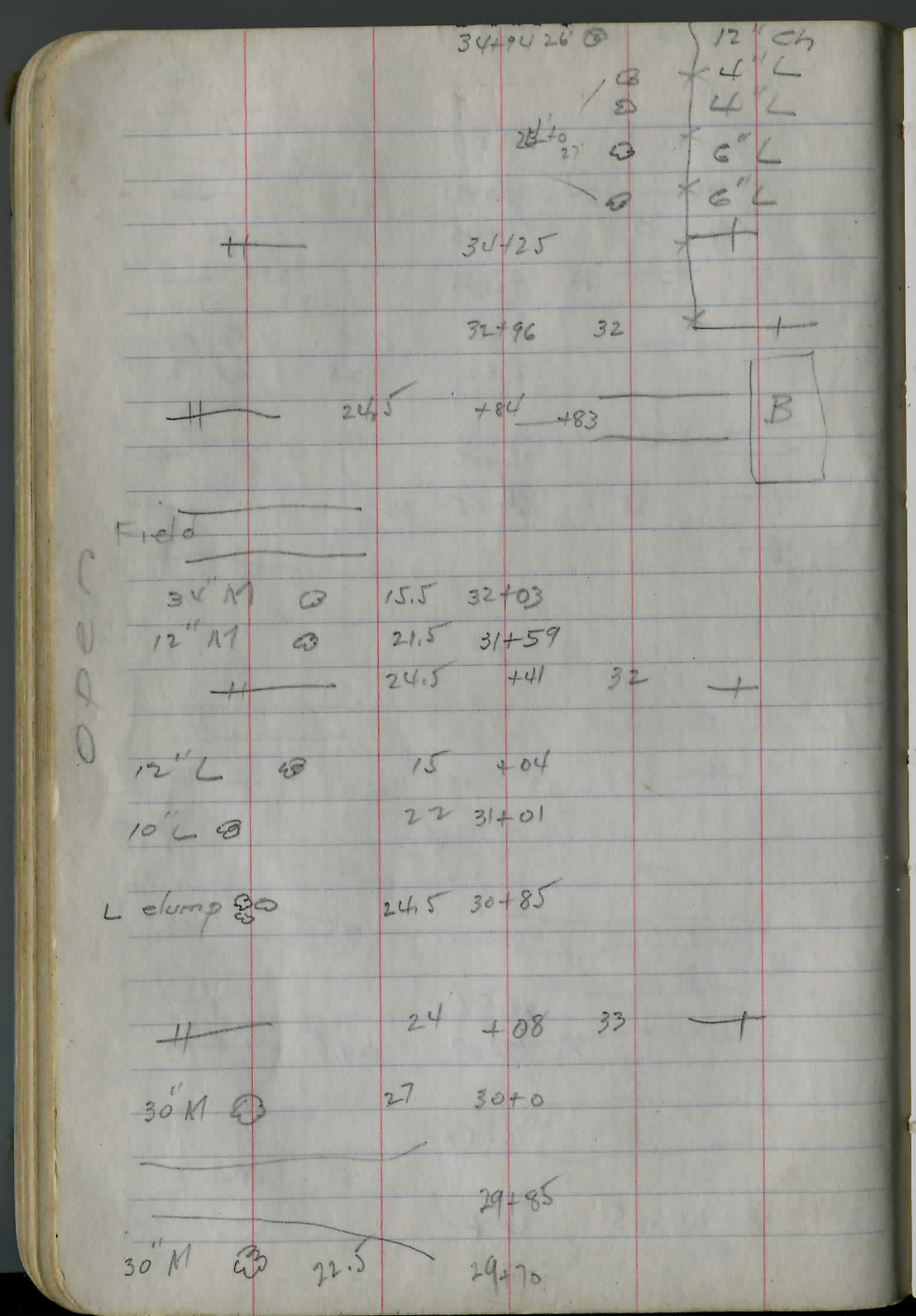
29.5 +21

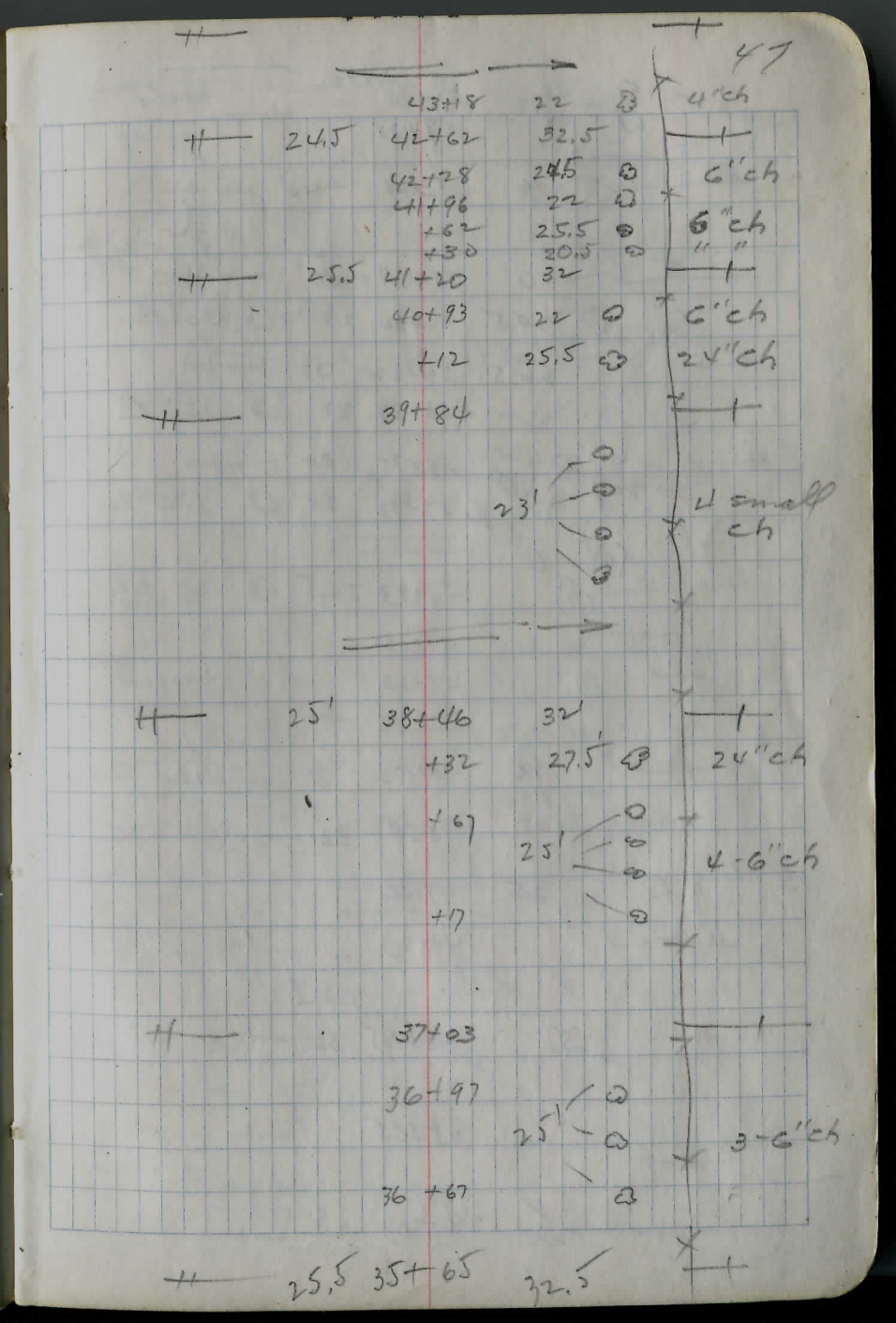
26" M 18' 5+0

+76 29


6" L
26.5
18+20
13.5
6" L
+71
+64
27.5
17+54
30.5
16+95
16+56
28" map
28
28
16+04
29.5
27.5
15+94
29.5
15' +28
N+65
21.5
12" L
N+55
22
12" E
BEGE
28
13+24
29
12+32 ± 31
30.5
12+90 ±35'
29'
+74
28
12+72
10+35
10+37
28
30.5


24
28+75
24" Ap
29' +45
25
27+35
33
33
+06
27+0
28
12" W
26+06
25
25+65 ✓ 32'
27 2 +84
30.5
Barn
20+97
20+48 ✓
27
19+07
29.5
18+58 ✓
15'
4" E
28" W
25'
18+36


34+94 26
12" ch
4" L
4" L
6" L
6" L
35+25
32+96 32
24.5
+84
+83
B
Field
3" M
15.5 32+03
12" M
21.5 31+59
24.5 +41 32
12" L
15 +04
10" L
22 31+01
L clump
24.5 30+85
24 +08 33
30" M
27 30+0
29+85
30" M
22.5
29+70

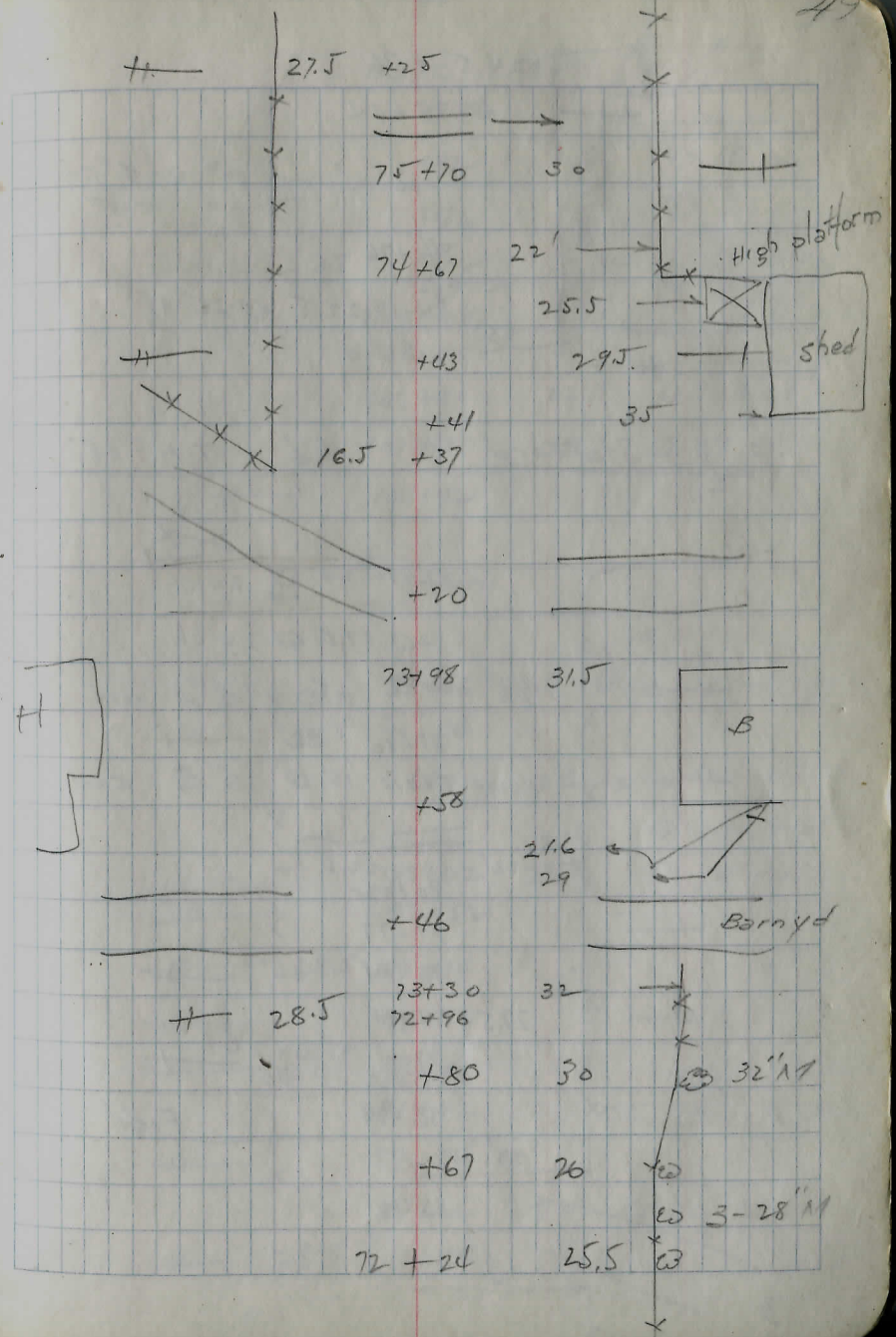

47
43+18 22
4" ch
24.5 42+62 32.5
42+28 24.5
6" ch
41+96 22
+62 25.5
6" ch
+30 20.5
25.5 41+20 32
40+93 22
6" ch
+12 25.5
24" ch
39+84
23'
4 small ch
25' 38+46 32'
+32 27.5
24" ch
+67
25'
4-6" ch
+17
37+03
36+97
25'
3-6" ch
36 +67
25.5 35+65 32.5

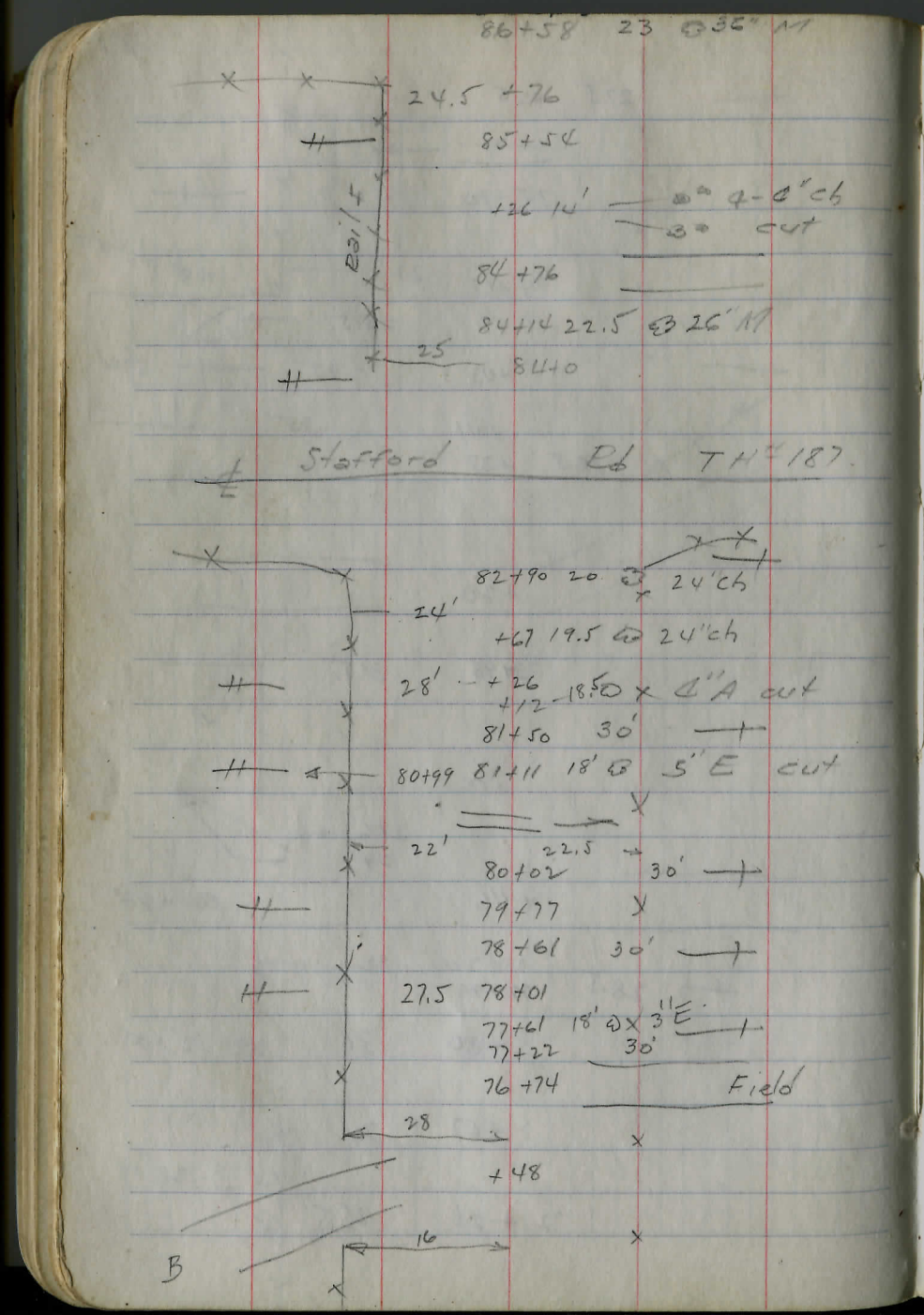
Big stumps 18 58+10 58+26 Field
18' 58+75
21'
16 57+08 +40'
CE/Anch & Tel
26.5
16' 55+67 ± 40'
29.5 +30 28 30" A
26.5 54+22 33
52+79 27 15" E
27' 52+75 32
30' 52+72 28 36" ch
Topo taken on curve
51+93 26.5 36" ch
51+33
51+23
26 49+72 31
+58 32
15" M 25 49+66
48+23
32.5
25 46+85 32
45+65
23 44+03 32.5

Begin Woods & brush

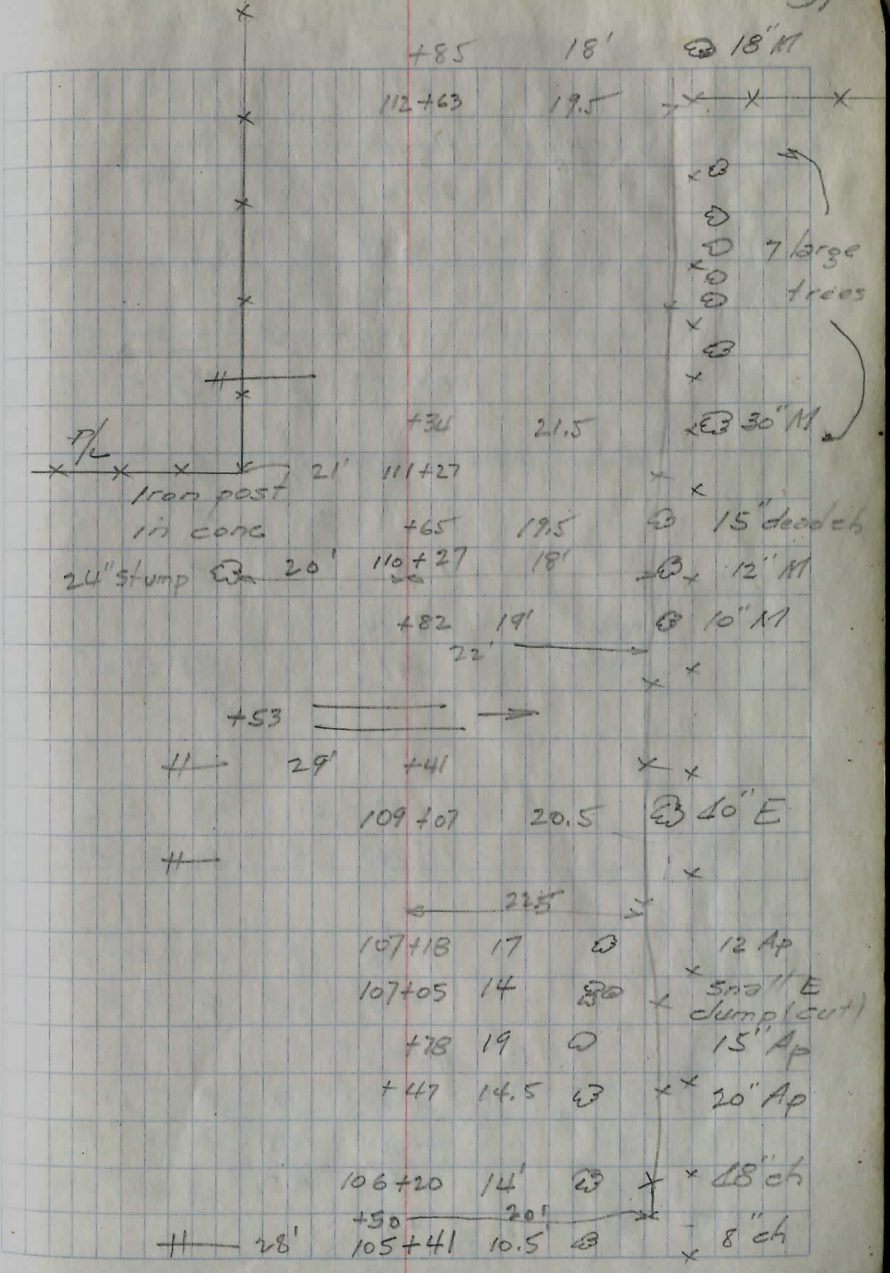
open

20' 71+93
+59 25.5'
+45
5-28" M
71+04 25'
70+80 25'
24.5 70+0 20'
31.5 69+0 20'
16 dead man
25'
68+0 27'
67+0
24 P
18.5 I
15 dm
+45
+33
Big St 25 65+07 ±22' ch. clump cut
25 28'
27' 64+06 30'
64+03
27 29.5
22.5 62+65 30.5
4 or 5 stumps at 62+80 to 64+0
20'
Big St 23 60+06
25'
27 59+90 30'
29'
25' 58+50 33
21
58+35 30


27.5
+25
75+70
30
22'
High platform
74+67
25.5
shed
+43
29.5
+41
35
16.5
+37
+20
73+98
31.5
B
+58
21.6
29
+46
Barnyd
73+30
72+96
32
28.5
+80
30
32"
+67
26
3-28"
72+24
25.5



103+95 22
+86
+72 15 ⊖ 15" pop
+46 17 ⊖ 26"ch
28 +42 24 ⊖ 15" pop
+17
103+08 13' ⊖ 18" pop
+90
102+80 22.5 ⊖ 18"ch
101+51 19 ⊖ 28" st.
101+42
100+01
18" stump
99+56 23.5 ⊖ △ P/L
28.5 99+44
+30 24 ⊖ 12" Wal
+10 24 ⊖ 12" Wal
99+02 23.7 ⊖ 14" Wal
97+52
28.5 95+54
93+53
28.5 91+52 P/L
91+42 Brush row
89+54
87+64 24 ⊖ 26" M
28.8 +54


+85
18'
18" M
112+63
19.5
7 large trees
+34
21.5
30" M
P/L
21'
111+27
Iron post in conc
+65
19.5
15" dead ch
24" stump
20'
110+27
18'
12" M
+82
19'
10" M
22'
+53
29'
+41
109+07
20.5
40" E
22.5
107+18
17
12 Ap
107+05
14
small E clump (cut)
+78
19
15" Ap
+47
14.5
20" Ap
106+20
14'
18" ch
+50
20'
28'
105+41
10.5'
8" ch

Begin row big willers

121+12 21' (tree)

+98 22 (tree) 40" E

25

120+69 29' 25

119+05 21' (tree) 30" O

+85 22' (tree) 14" Pop

22'

+46 14' (tree) 30" O P/L

118+29 21' (tree) 50" O

+96 19.5' (tree) 12" A brush

+71 21' (tree) 8" ch

+43 21' (tree) 18 A

117+14 28' 23'

+97 24 (tree) E cl

4" E cut

+30 23.5 (tree) 12" E

116+22 21 (tree) 12" E

115+63 18' (tree) 15" M

+98 19' (tree) 30" M

+30 20.5 (tree) 18 A

30" M (tree) 15' 114+25 22.5

+94 19 (tree) 12" ch

+62 18.5 (tree) 24" ch

+55 18.5 (tree) 14" ch

+38 29

113+36 18' (tree) 26" M

17 131+09

+62 17.5 (tree) (clump 28' Tulip

130+30 22' (tree) 36" M

+99 27' (tree) 12" O

129+83 28.5 (tree) 16" ch

8' 129+41

12.5 127+85

24" H (tree) 22' 127+13

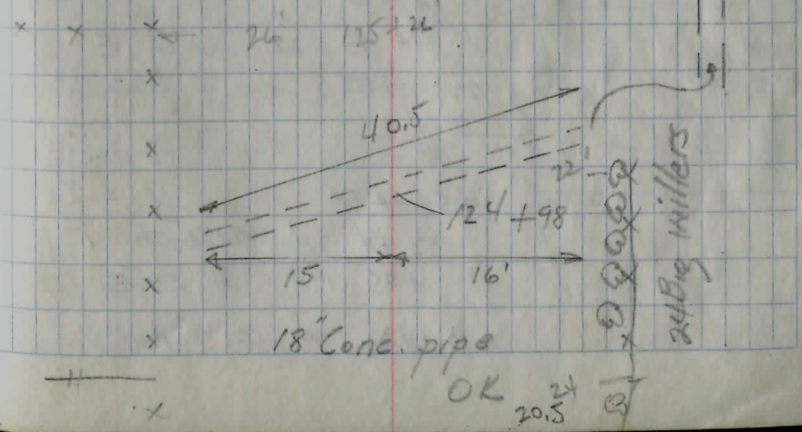
16" tree (tree) 20' 126+85

126+04.5

29 +91

29 125+85

℄ FRANKS RD 125+47



Bolge 139+27.8

1.8' 138+75 Pole 16 Fence 15

Mostly big willers

285 18' TEL

Begin tree row 18' 137+0 18'

24' 136+00 13.5

135+55

+71 9'

30"E 19 +59

12" M 19 +54

9" M 18 +36

12" M 22' 133+13

BELS

+93 28.5 15"E

12" M 22' +85

23'

19.5 +58

132+11 20' 16" ch

+85 19 30"E

131+32 10' 7" Wal

BRUSH

trees row 19' to 21' 152+0

22' +61

+38 19.5 18"E

+37 12.5

trees 21' 23.5' 150+0 17' 23.5 20" M fence

fence 21.5 148+03 15.5

147+78 19 15"E

to fence & trees 21 27' fence 146+0

+97 18' 10" M

+68 18.5

+65 19.5 15" M

+61 19.5 15" M

145+13 20' 15" M

+80 19' 25.5 24" M

+54 22.5 22.5 36"E

+25 17' 16" M

144+22 17' 24" M

143+39 20

Beg. tree row 21' 22'

+90 20'

22" M 20' 141+83

140+29 18.5

21' 17'

36" will 11.3 139+46

WOODS

166+49 15.5

30"E 30' 165+75

164+80 14

30" M & E ± 28 164+67

22" ch +95

22 ch 27.5 163+23

163+38 14'

28" M 26' 162+70

161+77 13.5

160+06 13

end fence 158+44 12.5

12" ch 24.5 157+60

12" ch 23.5 157+46

16" E 23.5 157+40

156+74 12.5

single wire fence

156+66 23'

155+10 13'

End tree row 21' 154+70

28.5

153+41 14 15" M

+76 12.5

152+23 17 24" M

CLEAR

WOODS

182+04

180+67 27.5

21.5 180+09

189+30

178+92 19'

H

177+19 23.5

23.5 175+99

+42 28.5

174+17

23 +87

173+62

+95 26

172+20 21 into field

23 171+73

170+18

20.5 +54

169+09 19'

CHICKS

+44 28

168+24 DE 18.5

20.5 +44

167+28 25 20" M

BELL ST

P/L 54

6" plum 26 192+24

6" ch 25 +90

191+0

22 +92

31.5

small evergreens & cherries +26'

190+43 Dr √

6" Ever 25 190+17

12" Ap 25.5 +57

+36 27

12" Ap 21.5 189+22

19 +95

10" Ap 21 +87

29 188+84 +62 188+64 Dr

18 187+57

17 186+05

12" Ap 15.5 +88 28

185+52

16 +60

184+12 Kettle

183+95

Loop

16 182+43 28.5

182+30 Dr

203+02

20" M 16.5 +56

2 - 14" E 21.5 +34

12" E 21.5 +31

15" M 26' +28

24" Ch 20' +16

201+02 29

200+43

WOODS

199+11

28' 198+12 28.5

197+23

196 +37 28'

Dr. Missing 196+06

Light brush Ed W sides Rd

195+53

194+60

30' 195+0

30' 193+76 Dr √

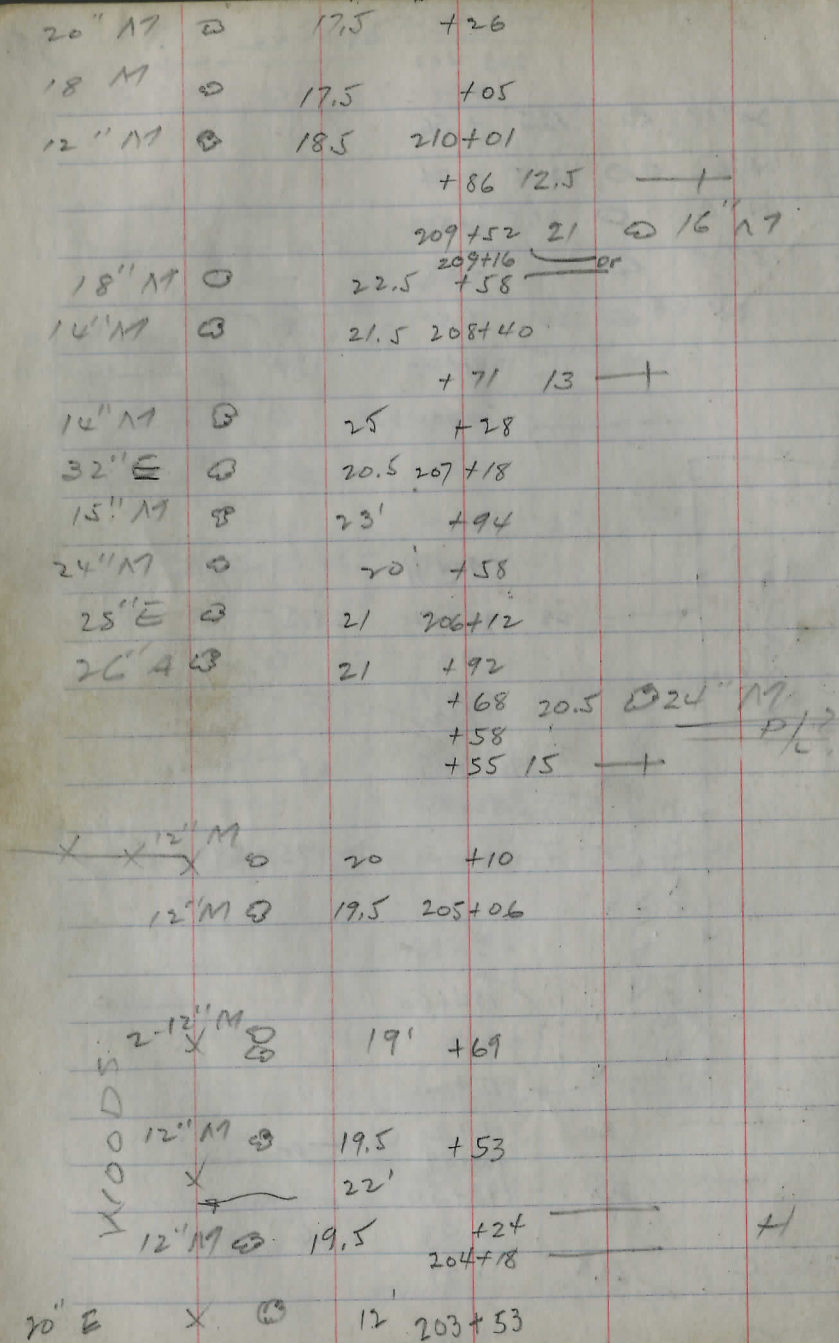
193+57

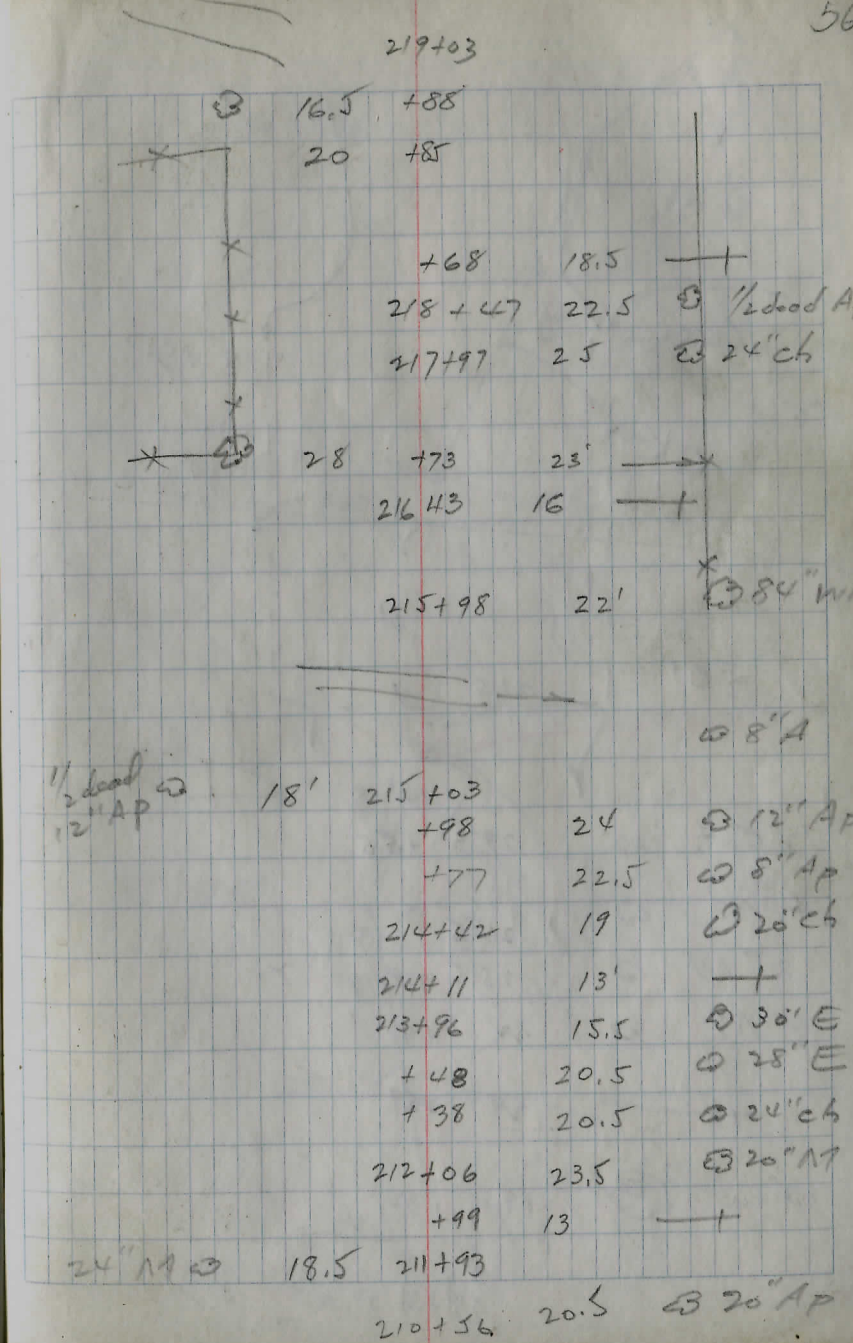
23 193+30

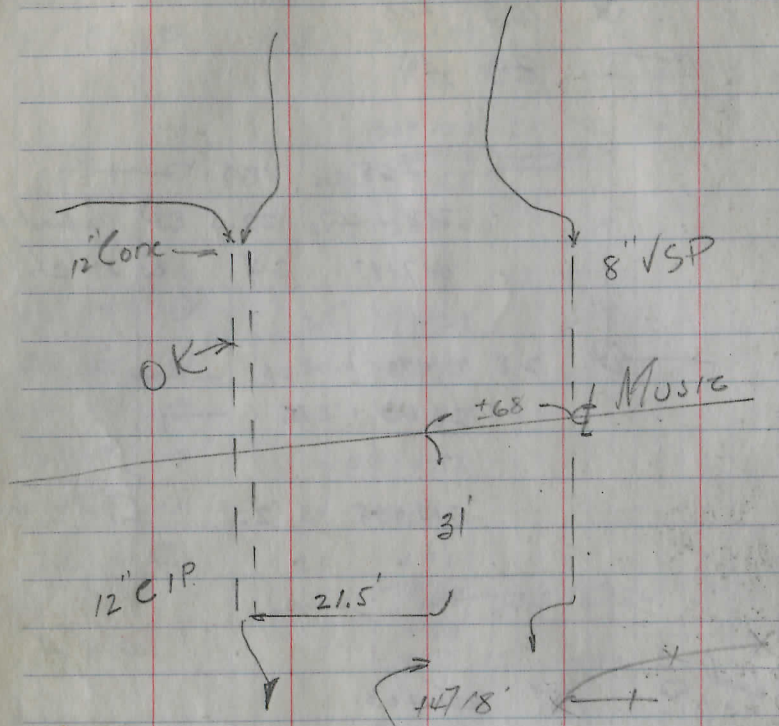
+83 26'

8" Ap 31.5 +77

8" Ap 26' +48


20" M
17.5 +26
18 M
17.5 +05
12" M
18.5 210+01
+86 12.5
209+52 21 16" M
209+16 or
18" M
22.5 +58
16" M
21.5 208+40
+71 13
14" M
25 +28
32" E
20.5 207+18
15" M
23' +94
24" M
20' +58
25" E
21 206+12
20" A
21 +92
+68 20.5 24" M
+58
+55 15
12" M
20 +10
12" M
19.5 205+06
2-12" M
19' +69
12" M
19.5 +53
22'
12" M
19.5 +24
204+18
+1
20" E
12' 203+53

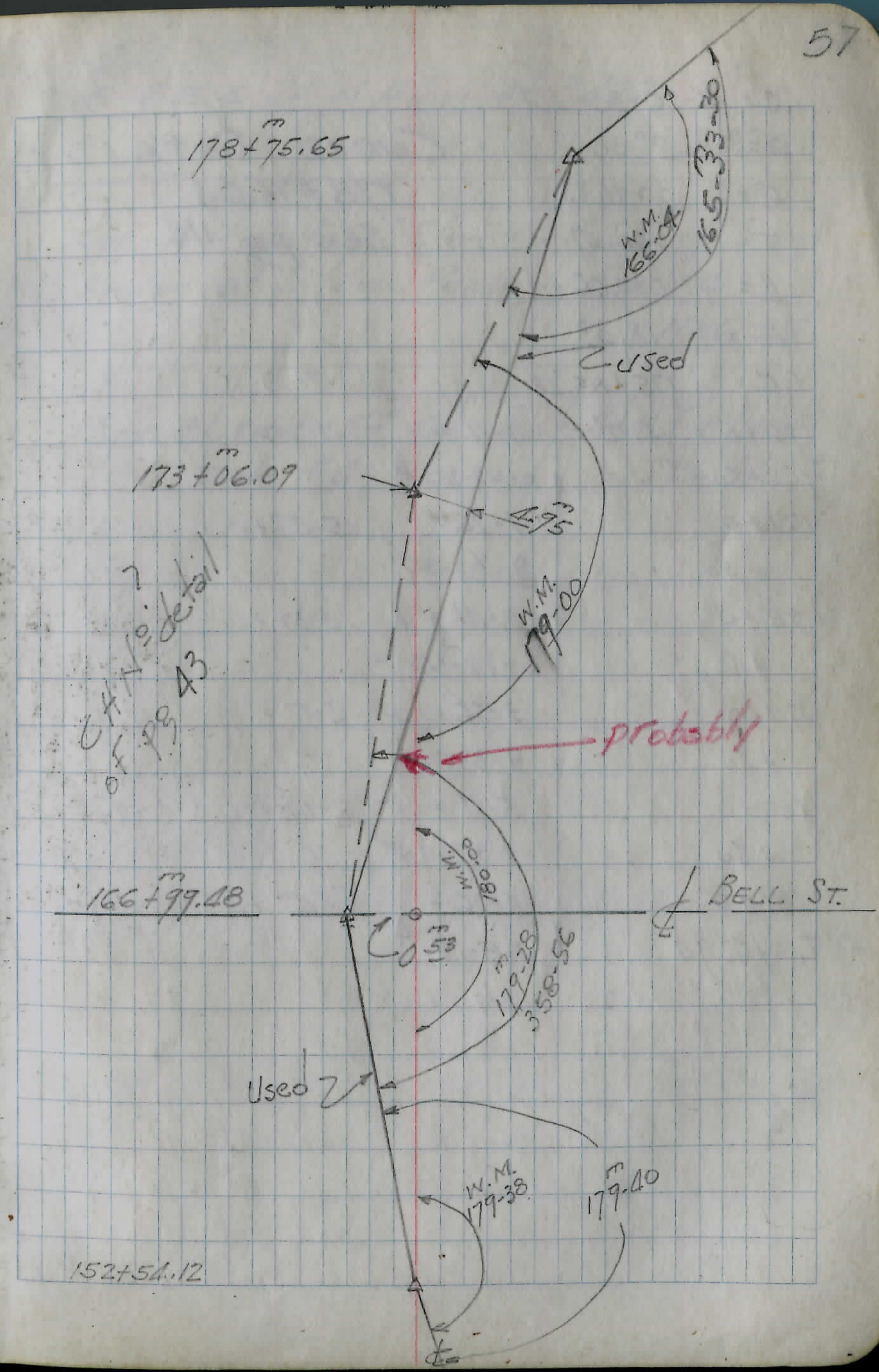

219+03
16.5 +88
20 +85
+68 18.5
218+47 22.5 1/2 dead Ap
217+97 25 24" ch
28 +73 23'
216 43 16
215+98 22'
84" Mill
8" A
1/2 dead 12" Ap
18' 215+03
+98 24 12" Ap
+77 22.5 8" Ap
214+42 19 20" ch
214+11 13'
213+96 15.5 30" E
+48 20.5 25" E
+38 20.5 24" ch
212+06 23.5 20" M
+99 13
24" M 18.5 211+93
210+56 20.5 20" Ap



12" Cot.	⊙	29.3	+56
4" Λ1	⊙	24.5	+38
8" Λ1	⊙	25.5	220+19
4" Λ1	⊙	22	+97
~~11~~		29	+59
shrub	⊙	18	+32

24

219+31 22.5 ⊙ 15" AP



Δ = 14-26-30 Rt

D = 2°-30'

R = 2291.83

T = 290.37

L = 577.66

E = 18.33

P.C. = 175+85.28

CURVE DATA
178+75.65
See pg 44

			7-13-15
176+0 =	14.72' =	0-11 +	7-02+
+50 =		0-48-30	
177+0		1-26 +	5-47+
+50		2-03-30	
178+0		2-41 +	4-32+
+50		3-18-30	
179+0		3-56 +	3-17 +
+50		4-33-30	
180+0		5-11 +	2-02 +
+50		5-48-30	
181+0		6-26 +	0-47 +
P.T. +62.94		7-13-15	

BM. No 1
X SE ∡ of N. Hdwl at #122

1232.03

Spk NW root 22" Elm ± 25' SE of S end bridge at S line Peabody (on #1)

1186.25

Spk N root 2nd Ch. S of Stafford Rd E side #1

1206.11 ±

LEVELS ON CH #4 FROM CH #10 SOUTH TO U.S. #422

	+	H.I.	−	ELV	Corrected elev.
B.M. #11	4.12	1214.49 ✓		1210.37	1210.37
T.P.	8.00	1215.75 ✓	6.74	1207.75 ✓	
T.P.	0.64	1209.81 ✓	6.58	1209.17 ✓	
B.M. #10			3.69	1206.12	1206.09
T.P.	0.69	1198.95 ✓	11.55	1198.26 ✓	
B.M. 9	0.11	1188.25 ✓	10.81	1188.14	1188.11
T.P.	12.39	1197.96 ✓	2.68	1185.57 ✓	
T.P.	7.48	1205.40 ✓	0.04	1197.92 ✓	
B.M. 8			4.09	1201.31	1201.30
T.P.	7.67	1206.77 ✓	6.30	1199.10 ✓	
B.M. 7	5.36	1210.46 ✓	1.67	1205.10	1205.09
T.P.	9.79	1216.25 ✓	4.00	1206.46 ✓	
T.P.	3.87	1219.47 ✓	0.65	1215.60 ✓	
T.P.	3.85	1216.55 ✓	6.77	1212.70 ✓	
B.M. 6	0.40	1207.38 ✓	9.57	1206.98	1207.01
T.P.	5.21	1206.79 ✓	5.80	1201.58 ✓	
B.M. 5	2.87	1204.41 ✓	5.25	1201.54	1201.58
T.P.	5.15	1201.23 ✓	8.33	1196.08 ✓	
T.P.	11.79	1212.06 ✓	0.96	1200.27 ✓	
T.P.	0.71	1210.37 ✓	2.40	1209.66 ✓	
B.M. 4			3.49	1206.88	1206.93
T.P.	7.48	1209.43 ✓	8.42	1201.95 ✓	
T.P.	12.62	1220.65 ✓	1.40	1208.03 ✓	
T.P.	10.34	1230.49 ✓	0.50	1220.15 ✓	
B.M. 3			1.68	1228.81	1228.89

Spk S.W. root 30" Pine 105' E of #4 on #10

Spk Set to E. Root 22" Cherry W Side Road ± 149+60

Spk [illegible] E Root 28" Fork Cherry W Side ± 143+50

Spk Set W. Root 20" Cherry E Side Road ± 129+80

Spk Set W Root 32" Maple E Side Road ± 115+00

Spk Set NWly Root 30" Cherry E Side Road ± 82+23
North [illegible]

Spk Set W Root 30" Maple E Side Rd 71+03.93 P.T.

1206.93
Spk E Side 28" S. Maple W Side Rd ± 49+46

Spk E Root (Ref Spk) 28" Maple W Side Rd 30+00 N Side drive

					Correct Elev
		1230.49 ✓			
TP.	0.98	1223.36 ✓	8.11	1222.38	✓
TP	2.38	1215.30 ✓	10.44	1212.92	✓
TP.	1.08	1203.54 ✓	12.84	1202.46	✓
TP	3.79	1194.54 ✓	12.79	1190.75	✓
BM. ✓			8.40	1186.14	1186.22
TP.	12.61	1206.80 ✓	0.35	1194.19	✓
TP.	12.76	1218.89 ✓	0.66	1206.14	✓
TP.	OK. 12.75	1231.56 ✓	0.08	1218.81	✓
TP.	5.50	1235.60 ✓	1.46	1230.10	✓
B.M 1			3.83	1231.77	✓ (1232.03)
				←	1231.84

Spk Set W Root 30" Elm E Side Rd 2.14+08

X in SE & N. Hdw 1 422 Culvert

PROFILE & SECT No 4 DE F

	+	H.I.			
B.M.	10.02	41.86 1241.79		1231.77	1231.84
Profile	South	(No. 4 C)			
BM	11.56	43.40 43.33		31.77	1231.84
"	East	(No. 4 2 2)			
T.P	12.80	55.09 55.02	1.21	42.12	
"	West	(No. 4 2 2)			
BM	7.25	39.02 39.02		31.77	1231.84
BM	1.22	33.06 1232.99		1231.77	1231.84
inlet FL	55		3.9	1229.2	
1					
2					
3					
4					

Elev. taken on curves
(9) = ± edge of pav't (9)
[2] = ± travelled ℄

X SEC N Hd'n'l

1232.51	33.9	36.6	37.3	36.7	36.5	36.2	34.3
9.35	7.99	5.3	4.6	5.2	5.4	5.7	7.6
	100	200	250	300	400	500	600

HI = 43.33 — 55.02 H.I.

33.2	35.2	38.1	42.1	47.03	51.3	53.3
10.1	8.1	5.2	1.21	7.99	3.7	1.7
100	200	300	400	500	600	700

31.9	31.6	31.4	31.8	32.5	34.5
7.1	7.4	7.6	7.2	6.5	4.5
100	200	300	400	500	600

← HI = 39.02

SQUARE FIGURES = ℄ of TRAVELED ROAD [7]
CIRCLED FIGURES = Edge of traveled roadway (7)

W ℄ E

31.1 / 1.9 / 30 (35) 1230.6 / 2.4 (18) 29.5 / 3.5 / 30

28.8 / 4.2 / 30 (4) 1229.6 / 3.4 28.5 / 4.5 / 30 (16)

27.4 / 5.6 / 30 (4) 1228.6 / 4.5 28.3 / 4.7 / 30 (16)

25.7 / 7.3 / 30 27.5 / 5.5 / (6) 1227.7 / 5.3 27.6 / 5.4 / (5) 29.2 / 3.8 / 27 29.3 / 3.7 / 35

1233.06
1232.99

	+	HI	−	Elev	
		DRIVE			
		Outlet PL	33 9.5	1223.49	
5					
6					
TP	2.10	1223.49	11.60	1221.39	
+31					DRIVE
7					
8					
TP	1.51	1214.49	10.57	1212.92	
9					
10					
11					

62

W E

25.5 1226.7
7.5 6.3
40

23.5
9.5

Note: Add 0.07 to pencil elev

25.8 26.0 25.0 1225.2 24.8 23.2 27.1 28.9
7.2 7.0 5.0 7.8 8.2 9.8 5.9 4.1
30 16 (7) (10.5) 15 20 35

20.8 21.7 1222.1 21.8 20.4 23.0 24.6
17.2 11.3 10.9 11.2 12.6 10.0 6.4
25 (9) (9) 13 18 35

19.8 1221.3
3.7 2.7
40

19.8 18.9 17.7 1218.4 17.4 15.6 20.2 21.6
3.7 4.6 5.8 5.1 5.6 7.9 3.3 1.4
35 24 15 (18) (19) 14 19 35

14.0 13.4 12.4 12.9 1213.5 12.9 11.5 13.9 14.2 13.5
9.5 9.9 11.1 10.6 10 10.6 11.8 9.6 9.3 10
35 16 11 (8.5) (13) 15 19 30 35

09.2 09.6 09.2 10.0 1210.0 10.2 8.7 10.5 10.4 11.5
5.2 4.8 5.2 4.4 3.8 4.7 5.7 3.9 4.0 2.9
35 14 11 (8.5) (13) 17 20 35 35

07.8 08.6 09.2 05.9 06.3 1206.7 06.2 03.8 10.1 11.0
6.6 5.8 5.2 8.5 8.1 7.7 8.2 10.6 4.3 3.4
35 20 14 9.5 (9.1) (18) 18.5 25 35

04.2 05.2 05.3 04.6
10.2 9.2 9.1 9.8
35 22 18 25 & 35

		1214.43			
TP,	0.15	1202.95	11.63	1202.80	
11+0					
12					
TP	2.96	1194.35	11.56	1191.39	
13					
14					
#2 BM 14+08			8.19	1186.16	use 1186.22
+36					BRIDGE
15+0					
16					
TP,	13.00	1204.07	3.28	1191.07	
17					

W E

1199^{7} 1200^{1} 1200^{6} 1199^{9} 1198^{2}

3.3 2.4 2.5 3.1 4.8

70 (8.5) (12) 16

95^{4} 95^{7} 93^{3} 93^{5} 1194^{3} 93^{5} 92^{1} 96^{8} 97^{5}

7.6 7.3 9.5 9.5 8.7 9.5 10.9 6.2 5.5

35 20 14 12 (13) (13) 14 17 24.5 35

84^{7} 90^{1} 90^{6} 90^{1} 89^{5} 90^{1} 88^{6}

9.7 4.3 3.8 4.3 4.9 4.3 5.8

35 (8.5) (11.5) 14 16 35

Add .07

83^{1} 84^{0} 89^{2} 89^{4} 88^{9} 84^{9} 86^{0} 85^{5}

11.3 10.4 5.2 5.0 5.5 9.5 8.4 8.9

35 22 (9) (11) 19 21 43 30

87^{0} 90^{4} 89^{0} 89^{1} 89^{0} 80^{4} 87^{0}

7.4 14.0 5.4 5.3 5.4 14.0 7.4

TOP OPENING F.L. HDWL HDWL FL TOP OPENING

Add .06

1188^{7}

5.7

94^{4} 93^{1} 89^{6} 90^{1} 90^{4} 90^{6} 90^{0} 88^{2} 88^{8}

0.0 1.0 4.8 4.3 4.0 3.8 4.4 6.2 5.6

35 25 17 18 13 (8.5) (11) 13 22 30

1195^{6}

8.5

	+	1204.07 −	Elv
18+0			
19			
TP.	12.29	1216.22 0.12	1203.95
20			
21			
+00			Culvert
22+0			
23+0			
TP.	12.96	1227.96 1.22	1215.00
24+0			
25			
26			

W

120.2^{1} 120.7^{1} 119.9^{2} 119.9^{6} 119.9^{8}

2.0 2.4 6.1 4.5 4.3

30 20 14 (9.5)

120.3^{5}

0.6

10^{6} 09^{3} 06^{5} 06^{8} 120.7^{2}

5.6 4.9 9.7 9.3 9.0

30 17 11 (8)

121.0^{3}

5.9

08^{4}

7.8

INLET F.L.

08^{1} 06^{3}

8.1 9.9

OUTLET F.L. 30' E of OUTLET

14^{0} 13^{6} 10^{2} 11^{4} 11^{9} 11^{5} 11^{8} 12^{1}

2.2 2.6 5.3 4.8 4.3 4.7 4.4 4.1 Drive

30 14 9 (7) (13.5) 15 30

121.2^{9}

3.3

16^{1} 15^{9} 13^{7} 14^{4} 14^{7}

11.9 12.1 13.3 13.6 13.3

30 13 18 (6)

$121.7.2$

10.8

23^{1} 22^{7} 19^{0} 19^{7} 20^{1}

4.9 5.3 9.0 8.3 7.9

30 15 8 (5)

E

119.9^{2} 120.0^{3} 119.9^{6}

4.9 3.3 4.5

(20) 15 30

06^{2} 08^{0} 07^{3}

9.5 8.2 8.9

(11.5) 16 30

14^{2} 14^{5} 14^{1}

13.8 13.5 13.3

(15.3) 16.5 30

19^{4} 19^{7} 18^{9}

9.4 8.3 9.1

(16) 20 30

27		1227.96			
28					
29					
TP.	5.76	1230.91	2.81	1225.15	
30					
B.M. #3		✓	2.09	1228.82	1228.81
		11-14-50			
B.M #3	0.56	1229.45 1229.37 ✓		1228.81	1228.89
31					
32					
33					
TP.	0.99	1217.99 ✓ 1217.91	12.46	1217.00 1216.92 ✓	
34					
35					

1222.4

5.6

26	25	24	24
2.0	2.8	3.9	4.0
30	8	4	(1)

1224.8

3.7

23	23	21
4.7	4.7	6.4
(15)	20	30

Add .06

25	1226.3	22	20
2.6	4.6	5.4	7.3
30		(19)	35

REF Spt EAST ROOT 28" MAPLE WEST SIDE ROAD & North Side of drive 30+00

11-14-50 FROST IN ROAD

1224.3

27.2	26.0	24.1	23.5	24.1	5.2
2.3	3.5	5.4	6.0	5.4	(1)
30	12	6	45	3	

24.5	23.9	21.9
5.0	5.6	7.6
[9]	[13]	30

Add .03

1222.1

3.9	4.7	7.6	7.4
30	95	5	[1]

1222.7

6.8	7.4	7.1	7.6
[8]	(13)	20	30

1218.9

7.4	8.0	11.3	10.6
30	10.5	5	(2)

1219.3

10.2	10.9	9.9	9.5
[7]	(15)	22	30

1215.8

2.2

1212.2

3.2	3.9	6.1	5.8
30	10	5	(1)

1212.5

5.5	6.3	6.9	5.0	4.6
[7]	(17)	19	22	30

1217.91 ✓
1217.99

	+	HI	-	EL	
36					
37					
TP	2.05	1208.44 1208.36	11.60	1206.39 1206.31 ✓	
38					
39					
+00					COLVERT
40					
+50					
41					
42					
43					

W E

1209.4
8.6

1207.2 1207.6

8.0/30 8.4/11 11.4/6 10.8/(2) 10.4/[6.5] 11.1/(16) 11.4/18 8.9/25 9.8/30

1206.0
2.4

1204.9
3.5/[7] 4.2/(6.5) 5.0/30

1204.7
3.6/30 3.4/15 5.65/10.5 5.7/9 3.7/6 3.7/(3)
FL. Field drain

1202.5
5.9/FL

1202.0 1201.0
6.4/FL 7.4
F.L FIELD DRAIN

1205.5
2.9

1205.6
2.8

1204.6 1205.1
0.5/30 1.6/13 4.3/7 3.8/(5) 3.6 3.3/[5] 4.1/(15.5) 3.1/18 3.6/30

1201.6
6.8

1199.4 1199.8
9.9/30 10.1/12 9.0/(5) 8.6 3.6/[5] 9.3/(15) 10.3/18 11.4/30

Sta.	+	H.I.	-	EL.	
		1208.36 1208.44			
43+79					CULVERT
44					
45					
46					
T.P.	7.94	1210.18 1210.10	6.20	1202.24 1202.16	
47					
48					
49					USE 1206.93
B.M. #4	(3.52)	1210.27 1210.27	3.34	1206.76	1206.88
50					
+98					CULVERT
51					

W — E

43+79: 95.5 / 12.9 F.L. & F. DRAIN 21' — 96.6 / 11.8 FL — 1199.2 / 9.2 — 96.1 / 12.3 FL — 94.9 / 13.5 F.L. F. DRAIN 23' — 92.6 / 15.8 100'

44: 1199.1 / 9.3

45: 99.7 / 8.7 / 30 — 99.7 / 8.7 / 19 — 99.4 / 9.0 / 11 — 99.7 / 9.7 / 9 — 1199.3 / 9.1 / (6) — 8.8 — 1199.7 / 8.7 / [3] — 99.1 / 9.3 / (14) — 98.7 / 9.7 / 20 — 97.7 / 10.7 / 24 — 96.7 / 11.7 / 30

46: 1201.1 / 7.3

47: 05.4 / 4.8 / 30 — 05.1 / 5.1 / 14 — 03.3 / 6.9 / 10 — 1204.1 / 6.1 / (7) — 5.7 — 1204.6 / 5.6 / [3] — (13) — 03.7 / 6.5 / 15 — 06.2 / 4.0 / 19 — 05.7 / 4.5 / 30

48: 1205.5 / 4.7

49: 05.8 / 4.4 / 30 — 05.5 / 4.7 / 12 — 04.9 / 5.3 / (10) — 05.0 / 5.2 / 8 — 1205.5 / 4.7 / [3] — 04.8 / 5.4 / (12.5) — 04.5 / 5.7 / 16 — 03.1 / 7.1 / 30

50: 1204.3 / 6.0

+98: 9.3 F.L. F. DRAIN 5 — 1201.0 / 9.3 F.L. — 1200.1 / 10.2 F.L.

51: 02.8 / 7.6 / 30 — 02.6 / 7.7 / 19 — 01.3 / 9.0 / 14 — 03.0 / 7.3 / 10 — 1203.3 / 7.0 / (7) — 6.8 — 1203.6 / 6.7 / [2] — 03.1 / 7.2 / (11) — 01.7 / 8.6 / 16 — 1199.9 / 10.4 / 30

	+	HI	−	ELV	
		1210.22 ✓ 1210.27			
52					
T.P.			3.30	1206.97 1206.92 ✓	

check levels BM 3 to B.M. 4

B.M. #3	0.47	1229.28 ✓		1228.81	
T.P.	1.88	1219.51 ✓	11.65	1217.63 ✓	
T.P.	5.16	1212.56 ✓	12.11	1207.40 ✓	
T.P. (37-38) 5/8			6.31	06.25	06.31
T.P.	9.54	1209.93 ✓	12.17	1200.39 ✓	
T.P. (dc-07) 5/8			7.75	02.18	02.16
B.M. #4			3.12	06.81	06.88
		1216.81		1206.97	
T.P.	9.86	1216.76		1206.92	
53					
54					
55					
56					

W E

07.8	06.3	04.5	04.6	1205.1	04.5	04.6	03.9	
2.5	4.0	5.8	5.7	5.2	5.8	5.7	6.4	
25	18	12	(7)		(13)	14	30	

1212.0	11.7		1208.0	08.3	1208.6	07.9	09.3	10.4	10.3
4.8	5.1		8.8	9.3	8.2	8.9	7.5 7.5	6.4	6.5
30	17	10	(8)		[2]	(12)	14 17	19	30

1214.0	13.7	1211.0		1211.5	10.8	12.2	11.9	12.7	12.5
2.8	3.1	5.8		5.3	6.0	4.4	4.9	4.1	4.3
30	13	(9)		[2]	(12)	15	17	18	30

09.7	09.4	08.4	08.9	1209.4		08.7	07.5	06.7
7.1	7.4	8.4	7.9	7.4		8.1	9.3	10.1
35	22	17 14	(11)	□		(10)	16	30

07.6	08.4	06.7	1207.5		1206.8	08.7	08.8	08.1
9.2	8.4	10.1	9.3		10.2	8.1	8.0	8.7
35	145	(9)	□		(11)	16	21	30

	+	HI	-	Elev	
		1216.76			
		1216.81			
57					
TP.	0.67	1205.01	12.37	1204.44	
		1204.96		1204.39	
58					
59					
60					
61					
+37.3					CULVERT
TP.	4.06	1200.51	8.56	1196.45	
		1200.46		1196.40	
62					
63					
+50					
64					
65					

W E

06.5 06.6 03.5 03.7 1204.2
10.3 10.2 13.3 13.1 12.6
30 12 6 (3) □

1203.3 06.4 06.8
13.5 10.4 10.9
(17) 24 30

02.0 01.8 00.5 1200.0 1199.6
3.0 3.2 4.5 5.0 5.4 4.8
30 18 13 8 (9)

1200.6
4.4
[4]

1199.6 1200.5 01.1
5.4 4.5 3.9
(15) 19 30

97.6 97.9 97.8
7.4 7.1 7.2 6.6
30 11 (9)

1198.5
6.5
[2]

97.7 97.4 96.7
7.3 7.6 8.3
(13) 16 30

96.0 96.2 96.8
4.0 3.8 3.2 7.8
30 11 (8)

1196.9
9.1

1197.3
7.7
[1]

96.6 96.3 96.3
8.4 8.7 8.7
(13) 14 30

1192.0 96.4 1196.7
13 8.6 8.3 8.4
P.L. H.W.L H.W.L

97.5 92.2 91.9
12.5 12.5 13.1
P.L. 100 200
13.5 91.5
300

92.9 93.4 95.9 1196.1 1196.6
7.6 7.1 4.6 H.W 4.0 3.9
30 17 10 (8) [2]

96.0 94.2 96.6
4.5 6.3 3?
(11) 16 20 30

1197.6
2.9
1198.1
2.4

1199.0 99.0 97.3 1198.0
1.5 1.5 3.2 2.5
30 14 (10) □

97.2 98.9 1199.0
3.9 1.6 1.5
(11) 14 25

1196.7
3.8

	+	1200.46 1200.51 H.I.	−	ELV	
66					
+75.5					CULVERT
67					
68					
T.P.	7.35	1205.88 1205.83	1.98	1198.53 1198.48	
69					
70					
71					
B.M. #5			4.31	1201.52	1201.58
72					
73					
74					

W

95.1 94.3 95.2 1195.8
5.4 6.2 5.3 4.7
22 16 12 (10)

92.3 1196.
8.2 5.0 4.5 3.6
F.L. H.W.I. H.W.I.

1196.0
4.5

95.3 94.8 96.0 1196.5
5.2 5.7 4.5 4.0
20+ 16 14 (11)

99.5 97.5 97.9 1198.6
6.4 8.4 8.0 7.3 7.6
23 19 (16) [14]

1201.9 1199.9 00.8 1201.4
4.0 6.0 5.1 4.5 5.2
21 16 (15) [5]

00.1 00.6 1199.9 00.8 1201.5
5.8 5.3 6.0 5.1 4.4
25 17 15 13 (11)

01.4 01.3 00.6 01.1 1201.6
4.5 4.6 5.3 4.8 4.3
30 18 15 (13) [7]

1201.7
4.2

01.8 01.5 01.7 1201.8
4.1 4.4 4.2 4.1
30 16 (9)

E

95.1 94.0 94.3 93.7
5.4 6.5 6.2 6.8
(10) 13 16 25

92.0 91.8 91.4
8.5 8.5 8.7 9.1
F.L. 100 200 300

95.7 94.9 95.5 95.9
4.8 5.6 5.0 11.6
(13) 12 14 30

1197.7 1200.5 00.6
8.2 5.4 5.3
(6) 16 30

1200.0 00.9 01.6 01.4
5.9 5.0 4.3 4.5
(6) 8 17 20 30

00.6 00.3 00.7 00.4
5.3 5.6 5.2 5.5
(10) 11.5 13 30

00.8 00.6 01.1 00.3
5.1 5.3 4.8 5.6
(10) 11 12 30

01.3 01.1 00.9
4.6 4.8 5.0
(10) 13 30

		1205.88 1205.83			
	+	H.	-	Elev	
75					
TP	2.80	1206.03 1205.98	2.65	1203.23 1203.18	
76					
+00					CULVERT
77					
78					
79					
80					
+68					CULVERT
TP,	8.06	1209.72 1209.67	4.37	1201.66 1201.61	
81					
82					
BM, #6			2.73	1206.94	1207.01

W E

1201.6
4.3

1200.5 1199.7 00.6 1201.0 00.4 1198.3
5.5 6.3 5.4 5.0 5.6 7.7
30 20 14 (9) (10.5) 30

1199.7 1198.3 1197.7 1197.2
6.3 7.7 8.3 8.8
FL. FL. 100 200
11 13

1201.2
4.8

01.9 00.2 1201.0 1201.5 00.7 00.3 00.2
4.1 5.8 5.0 4.5 5.3 5.7 5.8
30 22 13 10 (9) (11) 14 30

1201.6
4.4

1199.9 00.0 01.0 1201.5 00.8 1199.7 1199.5
6.1 6.0 5.0 4.5 5.2 6.3 6.5
30±25 12 (9) (10) 15 30

1199.3 1201.7 1198.9 1198.0
6.7 4.3 7.1 8.0
FL. FL. 100

1202.1
7.6

1204.0
4.4 5.7 6.5 6.9 6.1 5.7 6.5 6.5 5.7 6.5
30±25 16 13 11 (9) (11) 16 20 30

11-15-50 RAIN

	+	H.I.	−	ELEV	
B.M. #6	6.73	1213.74 / 1213.71		1206.98	1207.01
83					
+24.35					STAFFORD Rd
84					
T.P.	7.01	1218.59 / 1218.56	2.16	1211.58 / 1211.55	
+76					DRIVE
85					
86					
T.P.	6.48	1217.89 / 1217.86	7.18	1211.41 / 1211.38	
87					
88					
89					

W E

1207.2
6.5

07.0 6.7 C.L. S. CULVERT N. 6.6
06.3 7.4 C.L. S. CULVERT N. 6.6

12.2 1.5/600 | 10.7 3.0/400 | 10.0 3.7/400 | 09.8 3.9/300 | 09.9 3.8/200 | 09.4 4.3/100 | 1208.5 5.2 | 06.5 7.2/100 | 05.4 8.3/200 | 04.1 9.6/300 | 02.7 11.0/400 | 00.1 13.6/500 | 1199.7 14.0/600

10.5 3.2/30 | 10.6 3.1/16 | 09.7 4.0/12 | 10.3 3.4/(10) | 1210.9 2.8 [11] | 10.1 3.6 (8) | 1?.6 1.1/30

1212.6 6.0 | 14.9 3.7/45

13.4 5.2/30 | 13.7 4.9/21 | 11.2 7.4/14 | 11.8 6.8/(13) | 1212.6 6.0 [?] | 12.0 6.6/(6) | 6.6/9 | 16.1 2.5/22 | 16.3 2.3/30

10.1 8.5/30 | 09.8 8.8/15 | 10.9 7.7/(11) | 1211.6 7.0 [11] | 10.8 7.8 (8.5) | 11.7 6.9/14 | 12.4 6.2/30

1211.5
6.4

1211.4
6.5

(9) (11)

1212.1
5.8

	+	1217.86 1217.89 HI	−	Elv	
90					
91					
92					
93					
94					
TP	6.49	1220.80 1220.77	3.58	1214.31 1214.28	
95					
+69					Culvert
96					
97					
98					
99					
B.M.					

W — E

12.9 5.0 / 30 — 12.5 5.4 / 20 — 11.9 6.0 / 17 — 11.4 6.5 / 14 13 — 12.3 5.6 / (10) — 1213.0 4.9 — 12.3 5.6 / (12) — 11.3 6.6 / 14 — 13.2 4.7 / 18 — 12.5 5.4 / 30

1213.7 4.2

1213.8 4.1

(11) — (10.5)

1214.0 3.9

15.6 2.3 / 30 — 14.8 3.1 / 17 — 14.2 3.7 / 14 — 13.5 4.4 / 13 — 14.0 3.9 / (11) — 1214.5 3.4 — 13.8 4.1 / (10.5) — 13.5 4.4 / 30

1214.1 6.7

12.0 8.8 / 180 — 12.1 8.7 / 80 SW — 1211.9 8.9 / FL — 1214.2 6.6 — 11.6 9.2 FL — 9.2 — 11.5 9.3 / 100 NE — 08.1 12.7 / 200

1214.2 6.6

1214.5 6.3

2.7 / 30 — 18.1 3.7 / 17 — 17.3 3.5 / 14 — 15.3 5.5 / 9 (8) — 1215.8 5.0 [9] — 15.3 5.6 (11) — 15.9 4.9 / 15 — 15.1 5.7 / 30

1215.2 5.6

	+	H.I.	−	Elev.
		1220.77 1220.80		
100				
101				
102				
TP	0.24	1212.37 1212.34	8.67	1212.13 1212.10
103				
104				
105				
106				
107				
108				
109				
TP	4.64	1210.36 1210.33	6.65	1205.72 1205.69

1214.9
5.9
(8) (10)
1214.4
6.4

15.3 14.6 12.5 13.0 1213.7
5.5 6.2 8.3 7.8 7.1
30 19 12 (10)

12.9 13.1 13.3
7.9 7.7 7.5
(9) 72 30

1211.9
0.5

10.7 09.5 08.9 09.5 1209.9
1.7 2.9 3.5 2.9 2.5
30 21 17 11 (13) [11]

09.5 10.5 10.7
2.9 1.9 2.2
(7) 13 30

1208.3
4.1

1207.3
5.1
(10) (8)

1206.4
6.0

04.5 03.9 05.7 1206.2
7.9 8.5 6.7 6.2
30 19 15 14 (4)

05.5 04.5 04.2
6.9 7.9 8.2
(7) 12 30

1205.6
6.8

	+	1210.33 1210.36 HI	−	ELV	
109+53					CULVERT
110					
111					
112					
113					
114					
115		1208.14			1205.05
BM 7	305	1208.04	5.34	1204.99	(1205.10)
116					
103					CULVERT
117					
118					
400					HUMP

W E

1202.3 8.1 F.L. (10)
1205.4 5.0
1205.4 5.0
1205.6 4.8

1201.9 8.5 F.L. (10)
02.0 8.4 100
02.0 8.4 200
01.71 8.45 300

04.7 5.7 30
04.2 6.3 23
03.9 6.5 14
05.1 5.3 13 (13)
1205.6 4.8

04.8 5.6 (10)
04.2 6.2 13
04.9 5.5 15
04.7 5.7 18 30

1205.6 4.8
1204.7 5.7 (11)

(8.5)

1203.8 6.6

01.3 6.8 30
01.5 6.6 16
02.7 5.4 (11)
1203.2 4.9 Σ

02.6 5.5 (8)
01.7 6.4 12+16
02.3 5.8 17+30

1199.5 8.6 200 W
00.7 7.4 100 SW
01.3 6.8 F.L.
1203.2 4.9

01.5 6.6 F.L.

1203.3 4.8
1203.6 4.5 (9)
(10)
1203.7 4.4

	+	H.I.	−	Elev
		1208.04 1208.14		
119				
120				
	TP. 2.83	1205.14 1205.04	5.83	1202.31 1202.21
121				
122				
123				
124				
125				
124+98 ℄				CULVERT
125 +47.45				Franks Rd
126+04				CULVERT

W E

1203.4
4.7

00.6 01.3 00.3 01.3 1202.1
7.5 6.5 7.8 6.8 6.0
28 19 15 14 (10)

01.2 01.0 03.3
6.9 7.1 11.8 4.8
(10) 12 17 30

1201.2
3.9

1200.8
4.3

(9) (10.5)

1200.2
4.9

97.0 96.9 98.3 1198.8 98.3 96.8 98.4
8.1 8.3 6.8 6.3 6.8 8.3 6.7
30 25 13 (9) (9.5) 13 14 20 30

1199.4
5.7

1196.4
8.7
FL.

1196.1
9.0
FL

1195.7
9.4
100'N of Franks

+ H.I. − E
1.86 1248.90 1.00 05.04
02.7 08.0 10.7 10.3
12.2 6.9 4.2 4.6
600 600 400 300

08.3 00.8
1.8 4.3
200 100

1200.1
5.0

00.1 01.2 03.4 04.4 07.8 08.6
5.0 3.3 1.7 -1.3 -2.7 -3.5
100 200 300 400 500 600

1198.6
6.5±
FL.

1200.0
5.1

1198.0
7.1
FL

	+	HI	−	ELV	
		1205.04 1205.14			
127					
128					
129					
B.M. #8			3.84	1201.20	1201.30 (1201.31)
		11-16-50 RAIN			
BM #8	2.10	1203.40 1203.41		1201.30 1201.31	
130					
131					
132					
133		1200.17		1193.15	
T.P.	7.02	1200.18	10.75	1193.16	
134					
T.P.	1.37	1189.96 1189.97	11.58	1187.59 1188.60	

W — 1200.1 — E

91.4 1200.1 99.1 1199.4
3.7 5.0 6.0 5.7 5.0
27 13 10 (9)

1199.5 99.2 1200.3 00.5
5.6 5.9 4.8 4.6
(9.5) 11 14 30

03.0 1202.8 1199.5 1200.0 1200.5
2.1 2.3 5.6 5.1 4.6
30 14 6.5 (5) [4]

1199.8 1200.6 02.1
5.3 4.5 3.0
(13) 16 30

04.1 03.6 00.3 1200.5 1201.1
1.0 1.5 4.8 4.6 4.0
30 20 10 4 (3) [5]

00.4 02.6 02.1
4.7 2.5 3.0
(16) 20 30

02.4 1201.6 99.2 93.5 1199.1
1.0 1.8 9.7 4.9 4.3
30 13 7 6 (3)

1199.6
3.8
[6]

98.7 98.6 99.5 98.3
4.7 4.8 3.9 5.1
(18) 19 22 30

1200.3 99.0 97.0 92.4 97.0
3.1 4.4 6.4 7.0 6.4
30 15 12 11 (8)

1197.6
5.8
[11]

96.8 92.0 91.7
6.6 6.6 11.4 11.7
(10.5) 12 24 30

98.2 97.7 95.3 95.5 1196.2
5.7 5.7 8.1 7.9 7.2
30 19 13 12 (10)

95.6 96.2 90.7
7.8 7.2 13.7
(8) 12 35

1200.5 99.1 93.3 93.7 1194.4
2.9 4.3 10.1 9.7 9.0
35 24 15 (12) [7]

93.7 90.3 89.0
9.7 13.1 14.4
(6) 7 15 30

97.7 96.7 90.7 91.2 1191.7
2.5 3.6 9.5 9.0 8.5
35 26 17 (14) [5]

91.0 90.2 91.3 87.4 87.0
9.2 10.0 8.9 12.8 13.2
(9) 7.8 11 20 30

Sta.	+	H.I.	−	Elev.	
		1189.97 1189.96			
135					
+55					CULVERT
136					
137					
138					
T.P.	4.21	1187.63 1187.64	6.54	1183.42 1183.43	
139					
+36.8					Bridge
140					
141					

W E

87.1 87.0 87.8 1188.2 1187.7 86.6 85.6
2.9 3.0 2.2 1.8 2.3 3.4 4.4
30 20 (15) [5] (2) 6 15 & 30

1184.5 1.5 1187.4 1.4 1184.4
5.5 2.6 5.6
F.L. Hdwl Hdwl F.L.

83.8 84.4 84.2 85.9 1186.3 85.9 84.6 84.4 84.0
6.2 6.6 5.8 4.1 3.7 4.1 5.4 5.6 6.0
24.5 Channel 37 17 (11) [3] (6) 11 30 60

82.5 82.9 83.0 1184.8 84.2 84.3 82.9 82.5
7.5 7.1 7.0 5.2 5.8 5.7 7.1 7.5 7.5
24.6 Channel 44 11 (7) (10) 14 30 60

81.0 81.7 81.6 83.3 1183.8 83.2 82.0 81.3 80.9
8.0 8.3 8.4 6.7 6.2 6.8 8.0 8.7 9.1
30 16 9 (6) [2] (11) 14 30 80

80.8 80.9 83.1 1183.3 82.9 80.8 80.4 1179.6 80.2
6.8 6.7 4.5 4.3 4.7 6.8 7.2 8.0 7.4
30 12 (7.5) (8) 12 30 70

78.6 79.4 77.08 1183.11 76.8
9.0 8.2 10.55 4.52 10.8
F.L. 65 F.L. F.L.
130 Chan 2.7 H_2O 3' DEEP

80.6 81.5 82.1 1182.7 82.2 86.5 80.8
7.0 6.1 5.5 4.9 5.4 6.1 6.8
26 11 (7) [4] (11) 14 30

1183.7
3.9

		+	H.	−	Elev.	
			1197.64			
			1187.63			
142						
143						
143						
			1199.00		1186.34	
T.P.	12.66		1199.01	1.29	1186.35	
BM 9				10.93	1188.08	1188.11 (1188.14)
144						
145						
			1208.05		1197.93	
T.P.	10.12		1208.06	1.07	1197.94	
146						
450						
147						
148						
149						
BM 10	9.99		1216.11	1.01	1206.05	1206.09 (1206.12)

CONTINUED F.B. 157 PAGE 19

W E

94.3 85.1 84.9 84.1 84.8 — 1185.5 — 84.8 84.6 85.6 85.0
3.3 2.5 2.7 3.5 2.8 — 2.1 — 2.8 3.0 2.0 2.6
25 20 8 7 (5) — [4] — (14) 16 7.0 30

85.9 86.1 85.9 — 1187.2 — 86.2 87.2 87.6
1.7 1.5 1.7 — 0.4 — 1.4 0.4 0.4
20 9 8 (6) — [3] — (4) 17 20-14 30

90.5 90.3 90.2 1189.3 — 1190.1 89.2 89.0 89.4 89.1
8.5 8.7 8.8 9.7 — 8.9 9.8 10.0 9.6 9.7
30 21 10.9 (9) — [4] (14) 14 19.6 23 30

1200.2 95.6 96.0 — 1196.6 — 95.9 95.2 98.4 95.2
− 1.2 3.4 3.0 — 2.9 — 3.1 3.8 0.6 0.8
17 9 (6) — [3] — (11) 13 19.5 30

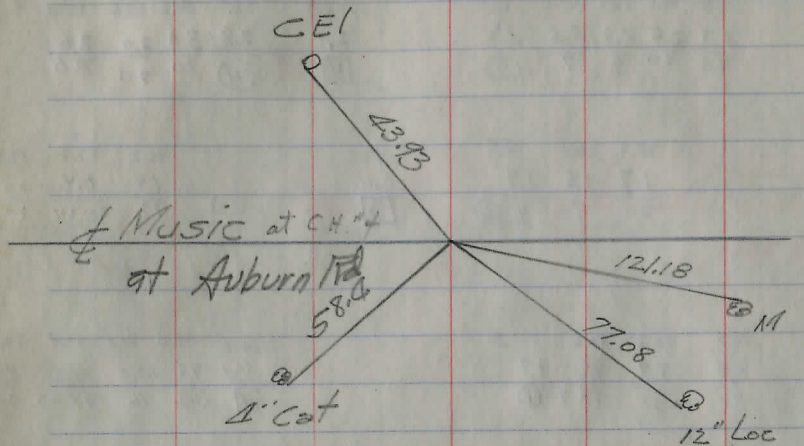
05.1 04.9 04.1 01.6 02.1 — 1202.9 — 02.0 01.7 03.5 05.0
3.0 3.2 4.0 6.5 6.0 — 5.2 — 6.1 6.4 4.6 3.1
30 21 16 10 (8) — [6] — (11) 12.5 15 30

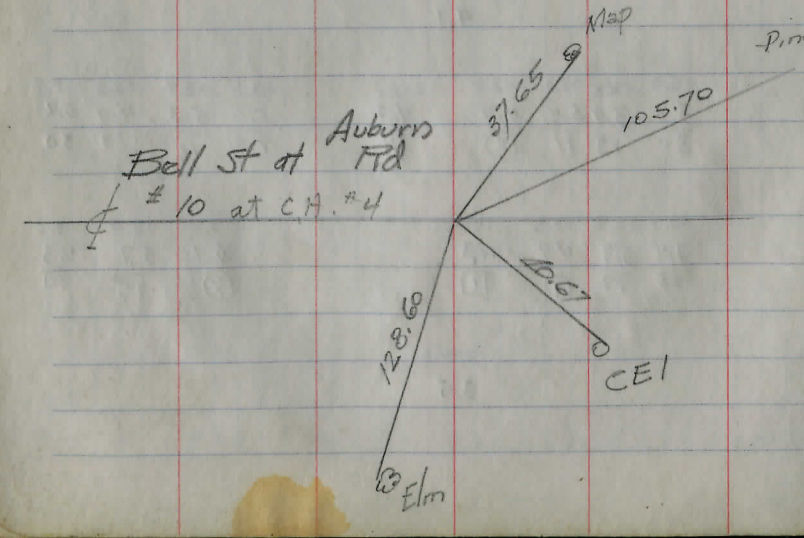
1204.0
9.1

05.0 04.2 02.7 03.2 — 1203.9 — 03.1 02.8 03.2 02.9
3.1 3.9 5.4 4.9 — 4.7 — 5.0 5.3 4.9 5.2
30 13 11 (8) — [1] — (9.3) 11 13 30

00.7 02.8 03.2 — 1203.8 — 03.0 02.4 03.8
7.4 5.3 4.9 — 4.3 — 5.1 5.7 4.3
28 12 (9) — [1] — (8) 15 30

1204.6
3.5





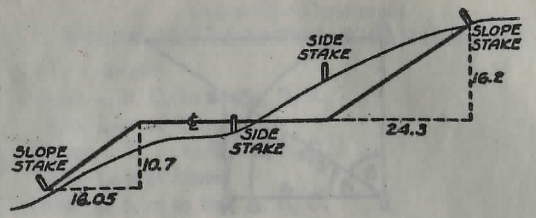


Table I.—Distances from Side Stakes for Cross-Sectioning

Slope 1½ to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

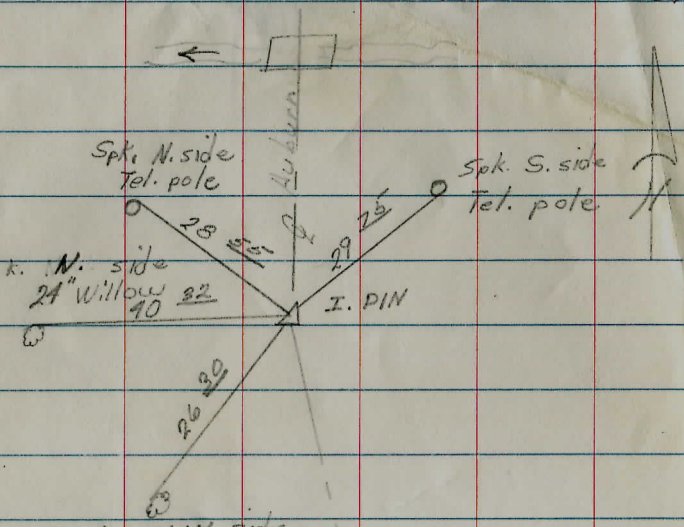
PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

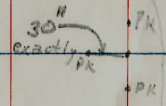
874.90 PI
269.60 PT
605.30

874.90

Auburn Rd. 1973

P.I. Reference for Sta 138+04.61





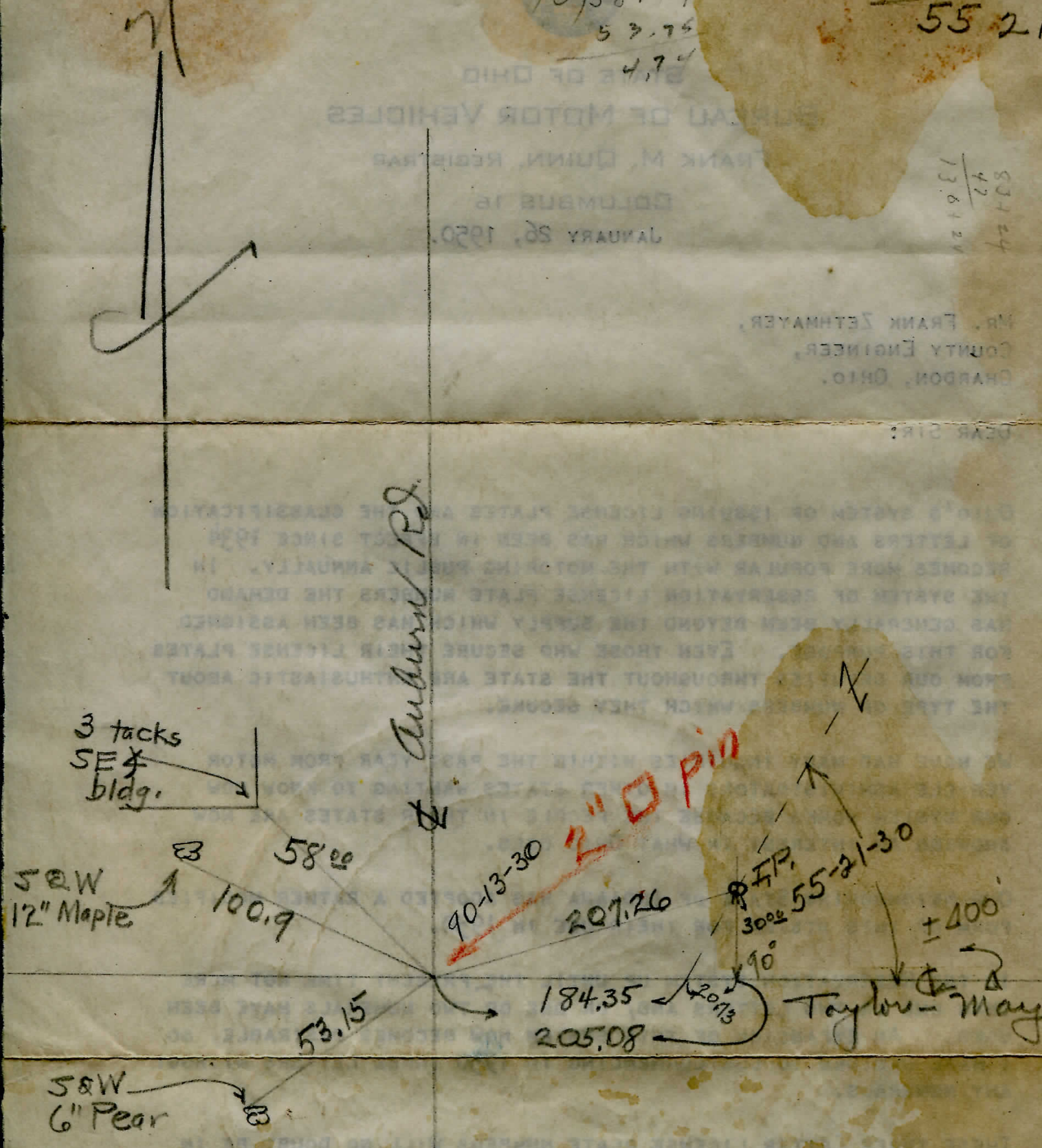
P.T. 129+30.58

Franks

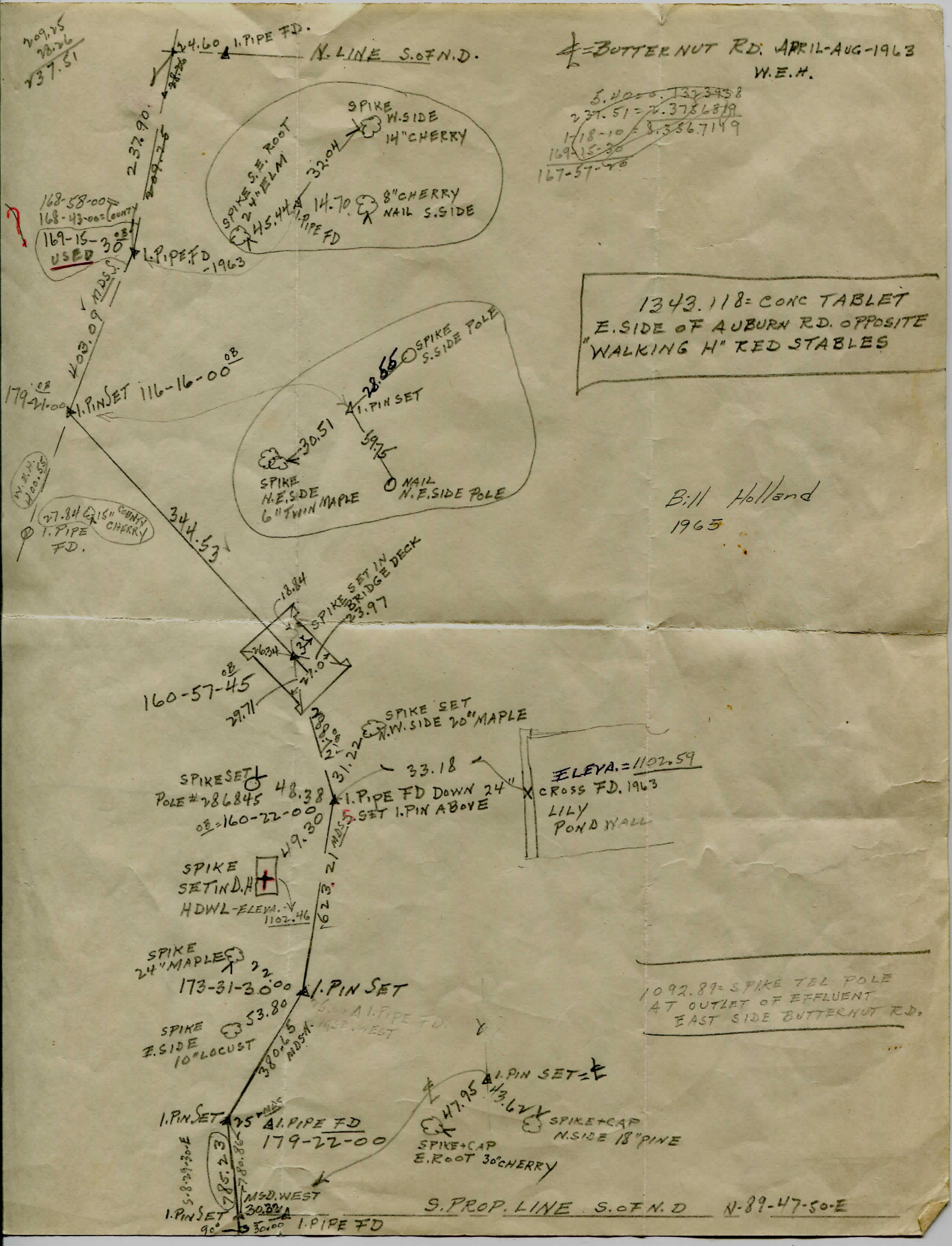
3.75 their
8.49 ours

614.88
10343.61
10958.49
53.75
4.74

90-07
34-45
55 21



3/8"ø Spike set ± 4' South of South edge of US 422 on ℄ of Auburn Road



℄ = BUTTERNUT RD. APRIL-AUG-1963
W.E.H.
N. LINE S. of N.D.
1. PIPE FD.
24.60
209.25
28.26
237.51
237.90
209.25
5.4020 = 1.3273938
237.51 = 2.3756819
1-18-10 = 3.3567149
169-15-30
167-57-40
SPIKE W. SIDE 14" CHERRY
32.04
SPIKE S.E. ROOT 24" ELM
45.44
14.70
8" CHERRY NAIL S. SIDE
1. PIPE FD
168-58-00
168-43-00 = COUNTY
169-15-30 OB
USED
I. PIPE FD -1963
MDS.
203.09
1343.118 = CONC TABLET E. SIDE OF AUBURN RD. OPPOSITE "WALKING H" RED STABLES
179-21-00 OB
1. PIN SET 116-16-00 OB
SPIKE S. SIDE POLE
28.56
1. PIN SET
30.51
59.76
SPIKE N.E. SIDE 6" TWIN MAPLE
NAIL N.E. SIDE POLE
N.E.H. 200.55
27.84
15" COUNTY CHERRY
1. PIPE FD.
344.53
Bill Holland 1965
18.84
SPIKE SET IN BRIDGE DECK
23.97
26.34
31
27.07
160-57-45 OB
29.71
38.7
SPIKE SET N.W. SIDE 20" MAPLE
31.22
33.18
ELEVA. = 1102.59
CROSS FD. 1963
LILY POND WALL
SPIKE SET
POLE # 286845
48.38
OB = 160-22-00
1. PIPE FD DOWN 24"
S. SET 1. PIN ABOVE
49.30
MDS.
N
SPIKE SET IN D.H.
HDWL - ELEVA. 1102.46
162.3
SPIKE 24" MAPLE
173-31-30.00
1. PIN SET
1092.89 = SPIKE TEL POLE AT OUTLET OF EFFLUENT EAST SIDE BUTTERNUT RD.
SPIKE E. SIDE 10" LOCUST
53.80
380.65 MDS.
MSD. WEST
1. PIN SET = ℄
47.95
43.62
SPIKE + CAP N. SIDE 18" PINE
SPIKE + CAP E. ROOT 30" CHERRY
1. PIN SET
.25 MDS
1. PIPE FD
179-22-00
S-8-29-30-E
785.23
780.86
MSD. WEST
30.32
S. PROP. LINE S. of N.D.
N-89-47-50-E
1. PIN SET
90°
30.00
1. PIPE FD